

# Finite Element Solution of Fluid- Structure Interaction Problems

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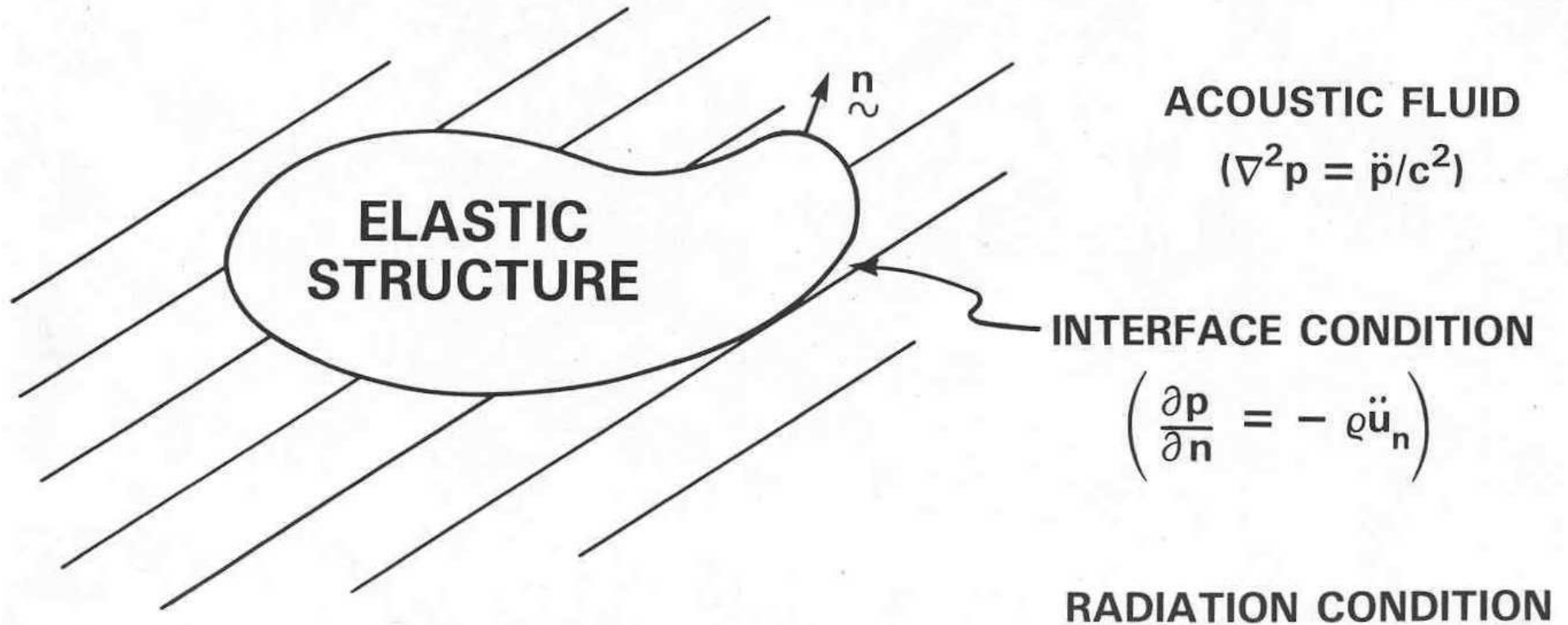
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# Fluid-Structure Interaction



Exterior Problems: Vibrations , Radiation and Scattering,  
Shock Response

Interior Problems: Acoustic Cavities, Piping Systems

# Structural Acoustics

Problems:      Radiation and Scattering  
                    (Time-Harmonic and Transient)  
                    Fluid-Loaded Vibrations  
                    Acoustic Cavities (e.g., Tanks, Pumps)  
                    Fluid-Filled Piping System Dynamics

Approaches:    Finite Element  
                    Finite Element/Boundary Element  
                    Finite Element/Infinite Element  
                    Doubly Asymptotic Approximations (DAA)  
                    Retarded Potential Integral Equation  
                    (Transient)

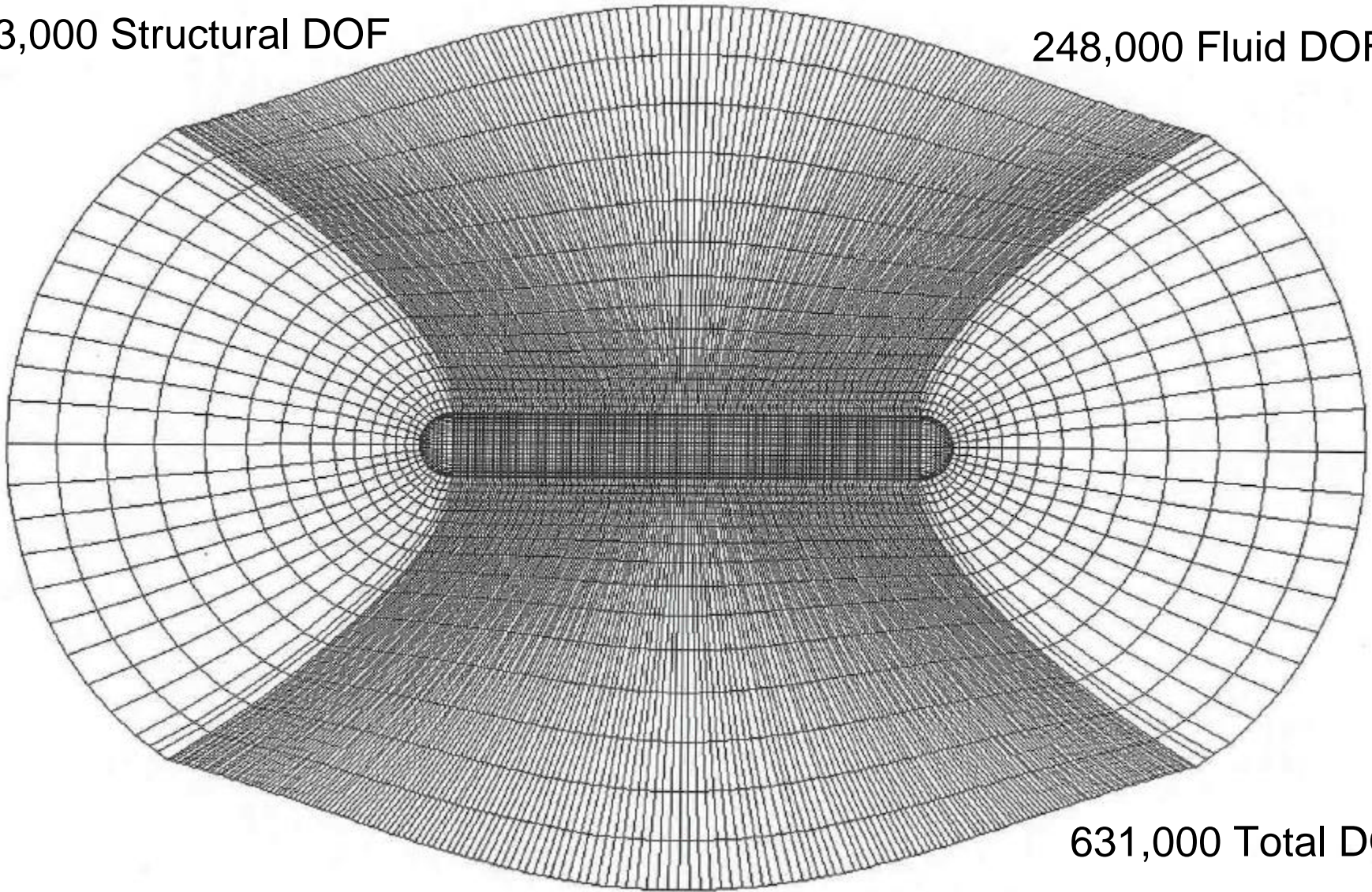
# Large-Scale Fluid-Structure Modeling Approaches

- Structure
  - Finite elements
- Fluid
  - Boundary elements
  - Finite elements with absorbing boundary
    - Infinite elements
    - $\rho c$  impedance
  - Doubly asymptotic approximations (shock)
  - Retarded potential integral equation (transient)

# Exterior Fluid Mesh

383,000 Structural DOF

248,000 Fluid DOF



631,000 Total DOF

# Structural-Acoustic Analogy

General Equation:  $\nabla^2 \phi + g = a \ddot{\phi} + b \dot{\phi}$

Navier's Equation of Elasticity:

$$\frac{\lambda + 2G}{G} u_{,xx} + u_{,yy} + u_{,zz} + \frac{\lambda + G}{G} (v_{,xy} + w_{,xz}) + \frac{1}{G} f_x = \frac{\rho}{G} \ddot{u}$$

$$\text{where } \lambda = \frac{E\nu}{(1 + \nu)(1 - 2\nu)} \quad (\text{Lamé constant})$$

Analogy:  $u = \phi, \quad v \equiv w \equiv 0, \quad \lambda = -G \Rightarrow$

$$G_e \text{ arbitrary, } E_e = \alpha G_e, \quad \rho_e = a G_e, \quad \alpha = \begin{cases} 10^{-5} & (2\text{-D}) \\ 10^{20} & (3\text{-D}) \end{cases}$$

$$F_x = f_x V = G_e g V - (G_e b V) \dot{\phi} \quad (\text{load} + \text{dashpot})$$



# Fluid-Structure Interaction Equations

**STRUCTURE:**  $M \ddot{u} + B \dot{u} + K u = -A p + f_1$

**COMPRESSIBLE FLUID:**  $\nabla^2 p = \ddot{p}/c^2, \partial p / \partial n = -\rho \ddot{u}_n$

$$Q \ddot{p} + H p = \rho A^T \ddot{u}$$

**COUPLED EQ:**

$$\begin{bmatrix} M & O \\ -\rho A^T & Q \end{bmatrix} \begin{Bmatrix} \ddot{u} \\ \ddot{p} \end{Bmatrix} + \begin{bmatrix} B & O \\ O & C \end{bmatrix} \begin{Bmatrix} \dot{u} \\ \dot{p} \end{Bmatrix} + \begin{bmatrix} K & A \\ O & H \end{bmatrix} \begin{Bmatrix} u \\ p \end{Bmatrix} = \begin{Bmatrix} f_1 \\ f_2 \end{Bmatrix}$$

**SYMMETRIC POTENTIAL FORMULATION:**  $q = \int p \, dt$

$$\begin{bmatrix} M & O \\ O & Q \end{bmatrix} \begin{Bmatrix} \ddot{u} \\ \ddot{q} \end{Bmatrix} + \begin{bmatrix} B & A \\ A^T & C \end{bmatrix} \begin{Bmatrix} \dot{u} \\ \dot{q} \end{Bmatrix} + \begin{bmatrix} K & O \\ O & H \end{bmatrix} \begin{Bmatrix} u \\ q \end{Bmatrix} = \begin{Bmatrix} f_1 \\ g_2 \end{Bmatrix}$$

# Fluid Finite Elements

- Pressure Formulation
  - $E_e = 10^{20}G_e$ ,  $\rho_e = G_e/c^2$ ,  $G_e$  arbitrary
  - Direct input of areas in K and M matrices
- Symmetric Potential Formulation
  - $u_z$  represents velocity potential
  - New unknown:  $q = \int p \, dt$  (velocity potential)
  - $G_e = -1/\rho$ ,  $E_e = -10^{20}/\rho$ ,  $\rho_e = -1/(\rho c^2)$
  - Direct input of areas in B (damping) matrix



# Finite Element Formulations of FSI

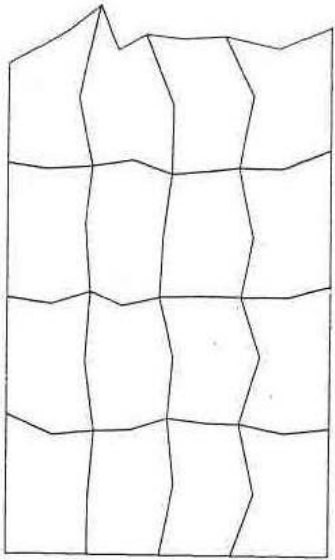
	Displacement	Pressure	Velo. Pot.
Fluid unknown	Total disp.	$p_s$	$q_s = \int p_s \, dt$
Fluid DOF/pt.	3	1	1
Coef. matrices	Symmetric	Nonsymmetric	Symmetric
Spurious modes	Yes	No	No
F-S interface cond.	MPC	Matrix entry	Matrix entry

+ 3-variable formulations

# Displacement Formulation

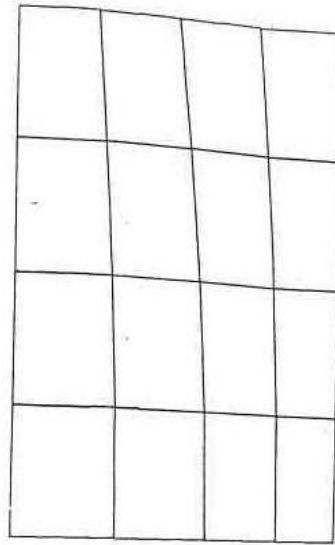
- Fundamental unknown: fluid displacement (3 DOF/point)
- Model fluid domain with elastic F.E. (e.g., elastic solids in 3-D, membranes in 2-D)
- Any coordinate systems; constrain rotations (DOF 456)
- Material properties (3-D):  $G_e \approx 0 \Rightarrow E_e = (6\varepsilon)\rho c^2$ ,  $\nu_e = 1/2 - \varepsilon$ ,  $\rho_e = \rho$ , where  $\varepsilon = 10^{-4}$
- Boundary conditions:
  - Free surface: natural B.C.
  - Rigid wall:  $u_n = 0$  (SPC or MPC)
  - Accelerating boundary:  $u_n$  continuous (MPC), slip
- Real and complex modes, frequency and transient response
- 3 DOF/point, spurious modes

# Displacement Method Mode Shapes



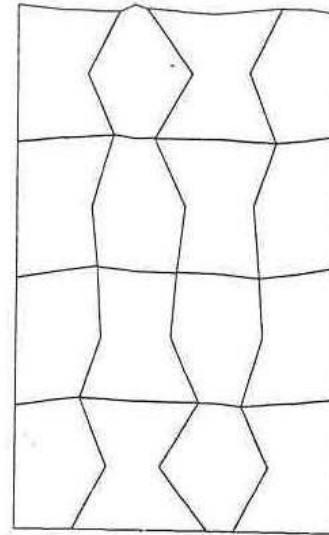
0 Hz

Spurious



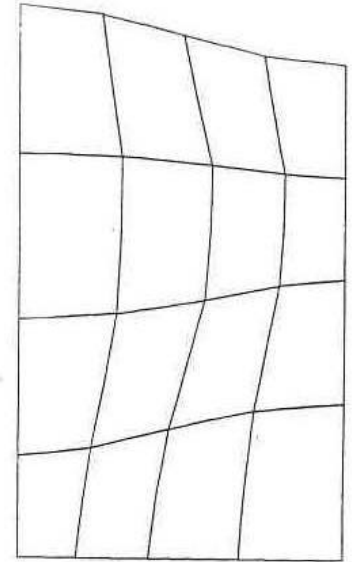
1506 Hz

Good



1931 Hz

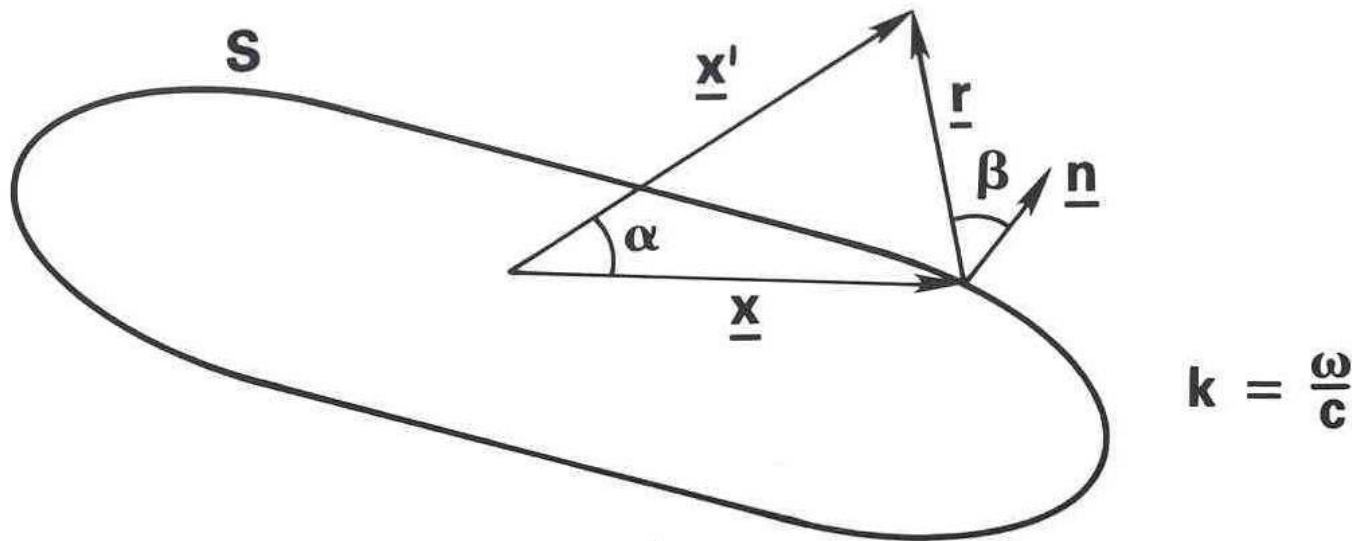
Spurious



1971 Hz

Good

# Helmholtz Integral Equations



$$\int_S \left( p \frac{\partial D}{\partial n} - \frac{\partial p}{\partial n} D \right) dS = \begin{cases} 1/2 p - p_I & (S) \\ p - p_I & (E) \\ -p_I & (I) \end{cases}$$

$$D = e^{-ikr}/4\pi r \quad (\text{GREEN'S FUNCTION})$$

$$\text{SURFACE: } Ep = Cv_n + p_I$$

# Matrix Formulation of Fluid-Structure Problem

Structure:  $Zv = F - GAp$

$$Z = (-\omega^2 M + i\omega B + K)/(i\omega)$$

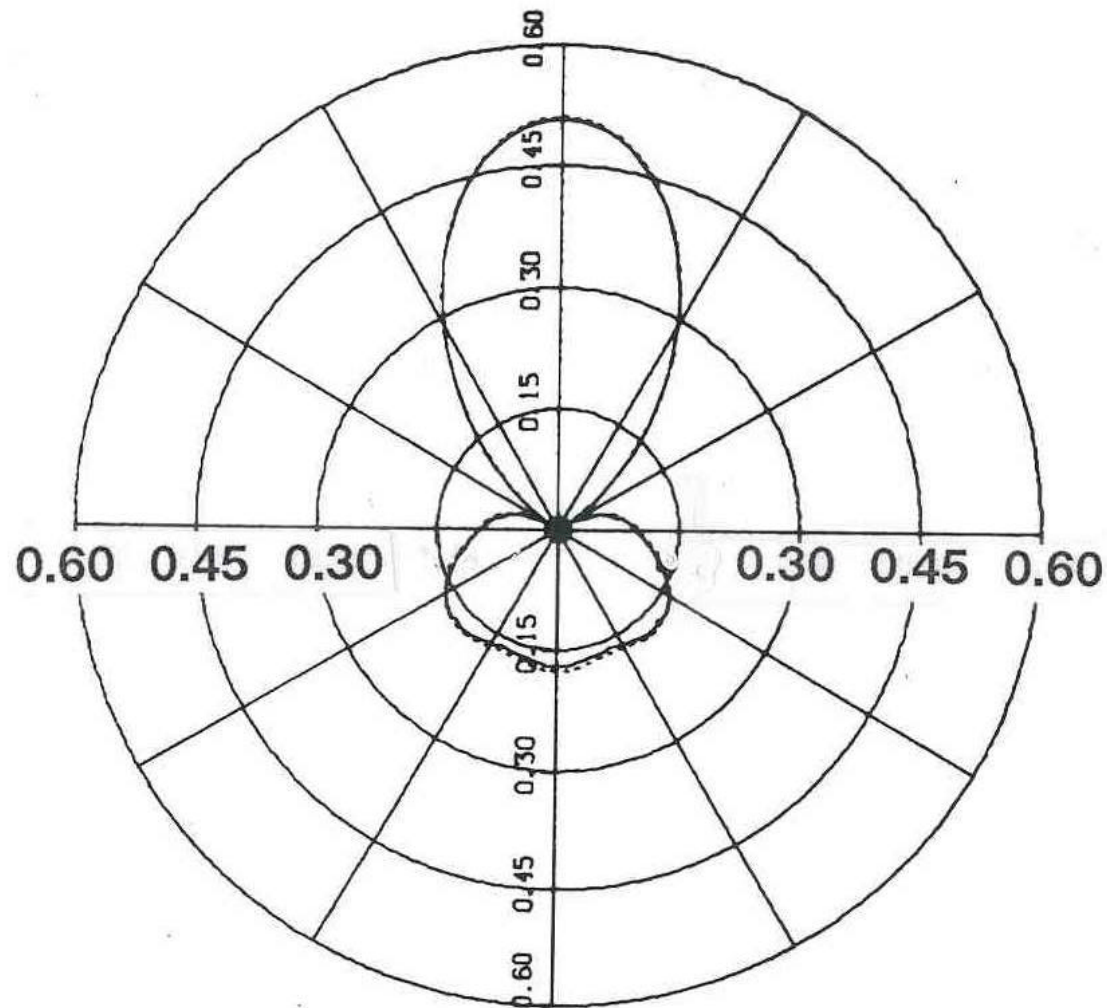
Fluid:  $Ep = Cv_n + p_i$

F-S Transformation:  $F = GF_n, \quad v_n = G^T v$

Coupled Equations:  $(E + CG^T Z^{-1} GA)p = CG^T Z^{-1} F + p_i$

Velocity:  $v_n = G^T Z^{-1} F - G^T Z^{-1} GAp$

# Spherical Shell With Sector Drive

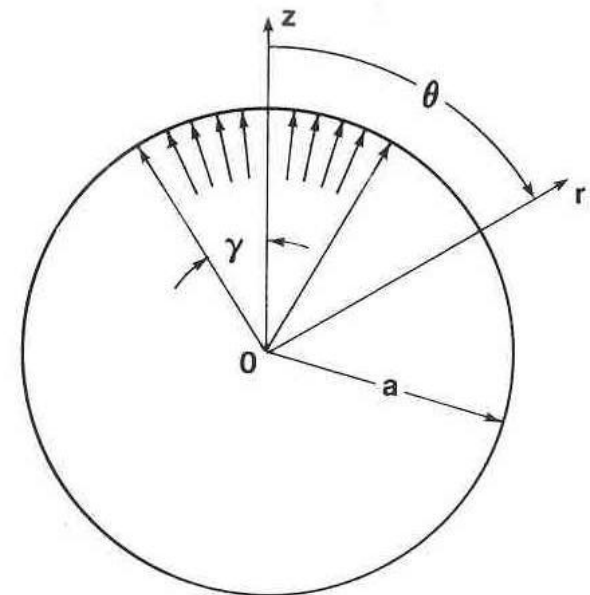


**FAR-FIELD PRESSURE**

$$\frac{|p|r}{p_o a}$$

$$k a = 5$$

— EXACT  
--- NASHUA



# Added Mass by Boundary Elements

Helmholtz equation: 
$$\oint_S \left( p \frac{\partial D}{\partial n} - D \frac{\partial p}{\partial n} \right) dS = \frac{p}{2}$$
$$D = \frac{e^{-ikr}}{4\pi r} \quad (\text{Green's function})$$

Boundary element equation: 
$$Ep = Cv_n$$

Added mass matrix: 
$$M_a = GAE^{-1} \left( \frac{C}{i\omega} \right) G^T$$

Eigenproblem: 
$$(M + M_a)\ddot{u} + Ku = 0$$



# Frequencies of Submerged Cylindrical Shell

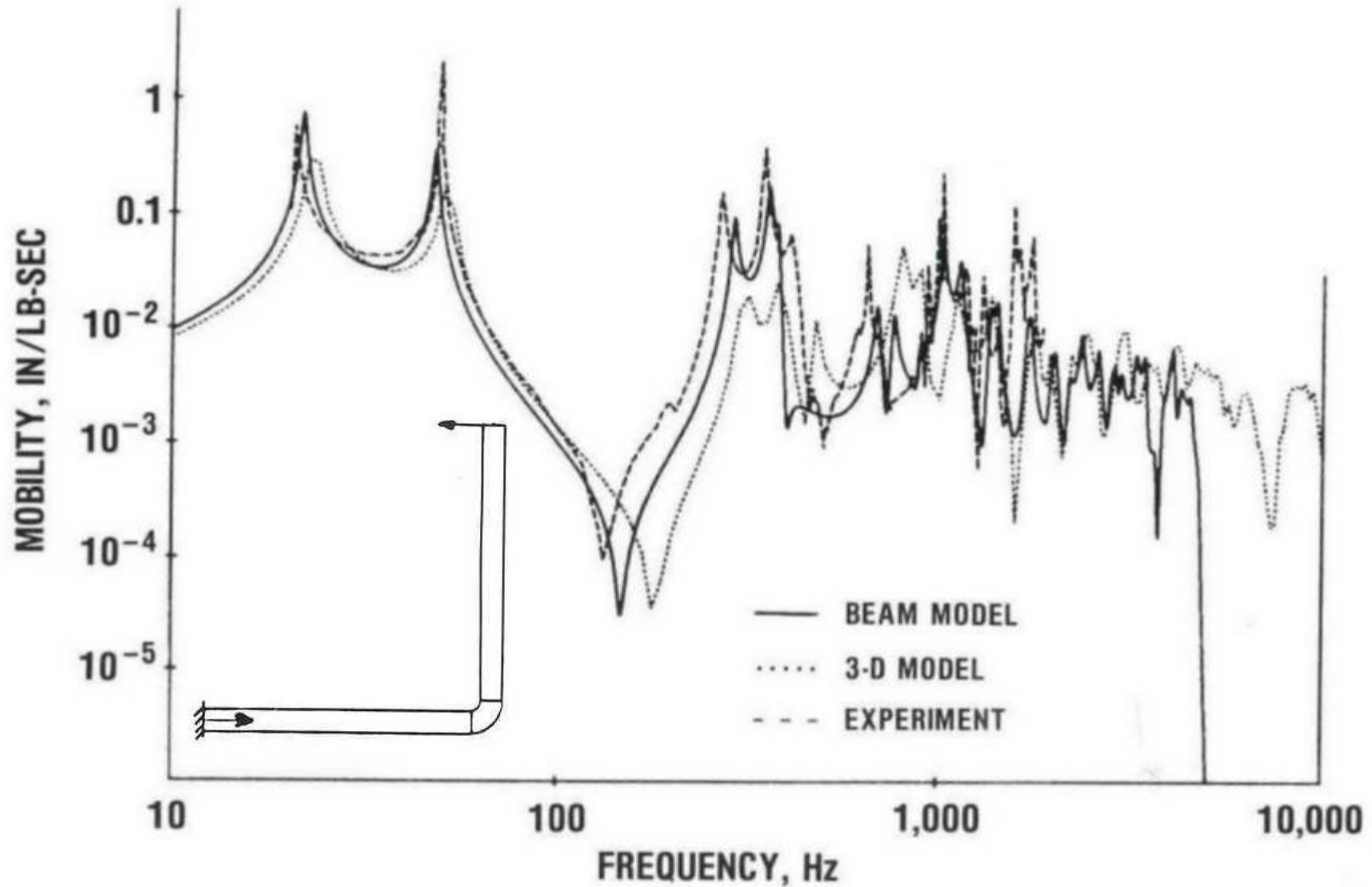
Mode	N	M	L	F.E.	B.E.	Approx.
1	1	0		0.00	0.00	0.00
2	2	1		1.13	1.13	1.11
3	0		1	1.63	1.44	1.38
4	3	1		1.79	1.81	1.77
5	4	1		3.61	3.67	3.57
6	1		1	4.44	4.26	4.22
7	4	3		4.81	4.82	4.70
8	3	3		4.94	4.93	4.82
9	5	1		6.31	6.38	6.18
10	5	3		6.83	6.86	6.67

N=circumferential, M=longitudinal, L=radial (end)

# Low Frequency F.E. Piping Model

- Beam model for pipe
- 1-D acoustic fluid model for fluid (rods)
- Two sets of coincident grid points
- Pipe and fluid have same transverse motion
- Elbow flexibility factors are used
- Adjusted fluid bulk modulus for fluid in elastic pipes  
 $E = B / [1 + BD / E_s t]$
- Arbitrary geometry, inputs, outputs
- Applicable below first lobar mode

# Planar Piping System: Free End Response



# Needs

- Link between CAD model and FE model
- Infinite elements
- Meshing (e.g., between hull and outer fluid FE surface)
- Modeling difficulties (e.g., joints, damping, materials, mounts)
- Error estimation and adaptive meshing

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