Miles’ Equation

Basics of Miles’ Equation.

- The following equation is attributed to John W. Miles.

\[
G_{RMS} = \sqrt{\frac{\pi}{2}} f_n Q [\text{ASD}_{\text{input}}]
\]

Where:
\[
f_n = \text{natural frequency}
\]
\[
Q = \frac{1}{2\zeta} = \text{transmissibility at } f_n \quad (\zeta \text{ is the critical damping ratio})
\]
\[
\text{ASD}_{\text{input}} = \text{input Acceleration Spectral Density at } f_n \text{ in } \frac{g^2}{Hz}
\]

In 1954, Miles developed his version of this equation for \( G_{RMS} \) (root mean square acceleration) as he was researching fatigue failure of aircraft structural components caused by jet engine vibration and gust loading. Miles simplified his research by modeling a system using one degree of freedom only. He also applied statistical advances that had been made at the time. While his goal was to analyze the stress of a component, the equation can be rearranged and used to determine, among others, displacement, force, and, in our case, acceleration.

- Single Degree of Freedom System

Miles’ Equation is derived using a single degree of freedom (SDOF) system (lightly damped), consisting of a mass, spring and damper, that is excited by a constant-level “white noise” random vibration input from 0 Hz to infinity. Miles’ Equation is thus technically applicable only to a SDOF system.

This figure shows a typical representation of a SDOF oscillator. The mass (m) is attached to the spring (stiffness k) and the damper (damping c). The system is forced by the random vibration function (F) in the y-direction only.

- SDOF System Response Plot

The plot shows the input and response of a SDOF system. Miles’ Equation calculates the square root of the area under the response curve, providing us with the well known \( G_{RMS} \) value.

- Response Parameters

Miles’ Equation can also be used to predict other response parameters such as stress or displacement. For example, the displacement equation for \( Y_{RMS} \) is given here.

\[
Y_{RMS} = \frac{Q [\text{ASD}_{\text{input}}]}{32\pi^3 (f_n)}
\]
USES OF MILES’ EQUATION

- **DESIGN** – During the design of a part, if enough analysis has been performed to determine the part has a predominant resonant frequency, then Miles’ Equation can be used to estimate the loads due to random vibration. Just calculate the $G_{RMS}$ value and multiply it by 3. That’s the “three sigma” load. Keep in mind, this is conservative.

- **TESTING** – Accelerations due to random vibration at resonant frequencies in a multiple degree of freedom system can be approximated using Miles’ Equation. This will indicate how much of the overall RMS acceleration is occurring at a resonant peak of interest compared to the complete frequency spectrum.

MILES’ EQUATION PITFALLS

- **MILES’ EQUATION DOES NOT WORK IN REVERSE** – Accelerations cannot be determined during random vibration testing using Miles’ Equation. An upper bound on loads can be calculated using the $3\sigma$ value, but that’s about it. In other words, a part designed to $3\sigma$ equivalent static loads will survive a random vibration test. However, Miles’ Equation cannot be used to predict the failure of a part designed to less than $3\sigma$ levels.

- **MILES’ EQUATION DOES NOT GIVE AN EQUIVALENT STATIC LOAD** – Calculating the $G_{RMS}$ value at a resonant peak after a random vibration test and multiplying it by the test article mass does not mean that the test article was subjected to that same, equivalent static load. It simply provides a statistical calculation of the peak load for a SDOF system. The actual loading on a multiple DOF system due to random input depends on the response of multiple modes, the mode shapes and the amount of effective mass participating in each mode. Static testing must still be done.

- **MILES’ EQUATION MAY NOT BE CONSERVATIVE FOR A SHAPED INPUT SPECTRUM** – Miles’ Equation is based on the response of a SDOF system subjected to a flat random input. If Miles’ Equation is used to calculate the $G_{RMS}$ response to a shaped input spectrum, the result will not accurately reflect the rigid body response below the resonant frequency. If the shaped input spectrum has high ASD levels below the resonant frequency, then Mile’s Equation may significantly underpredict the $G_{RMS}$ response. The following plot shows this condition. Note that the Miles’ assumption has a response of 31.8 $G_{RMS}$ while the actual SDOF response is much greater at 39.7 $G_{RMS}$. This demonstrates that Miles’ Equation is best used when the input ASD is flat or nearly so.

REFERENCES:


PREPARED BY:  
RYAN SIMMONS, SCOTT GORDON, BOB COLADONATO, NASA Goddard Space Flight Center, May 2001