

VIRTUAL DESIGN OF QUIET UNDERWATER SHELLS



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OUTLINE OF PRESENTATION



- ☑ Introduction
- ☑ Structural Acoustics of Underwater Stiffened Shells
- ☑ Virtual Reality Design of The Shells
- ☑ Performance of the Shells
- ☑ Conclusions
- ☑ Future Directions

OBJECTIVES

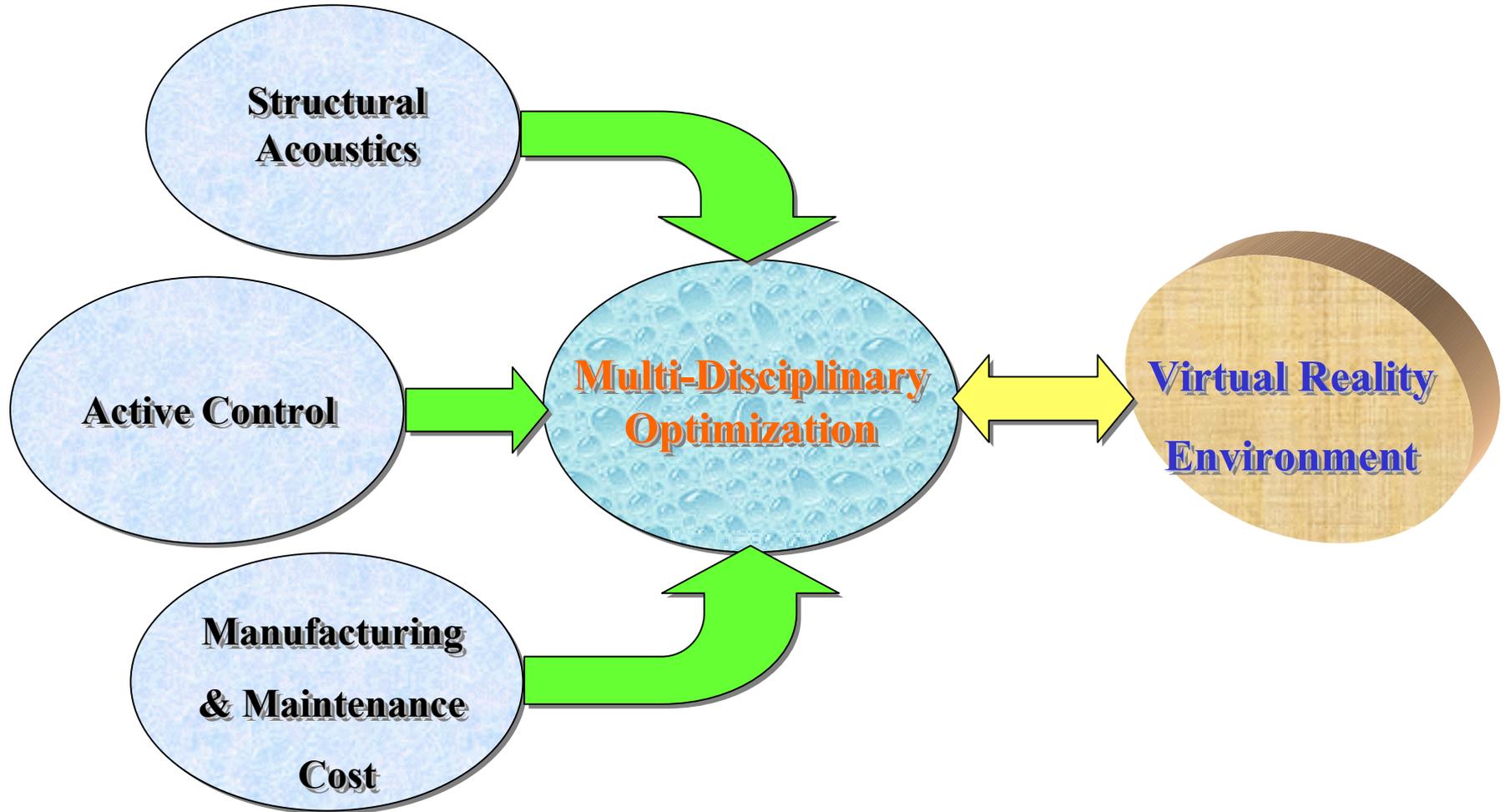


Design of Quiet Underwater Shells with Passive Stiffeners using:

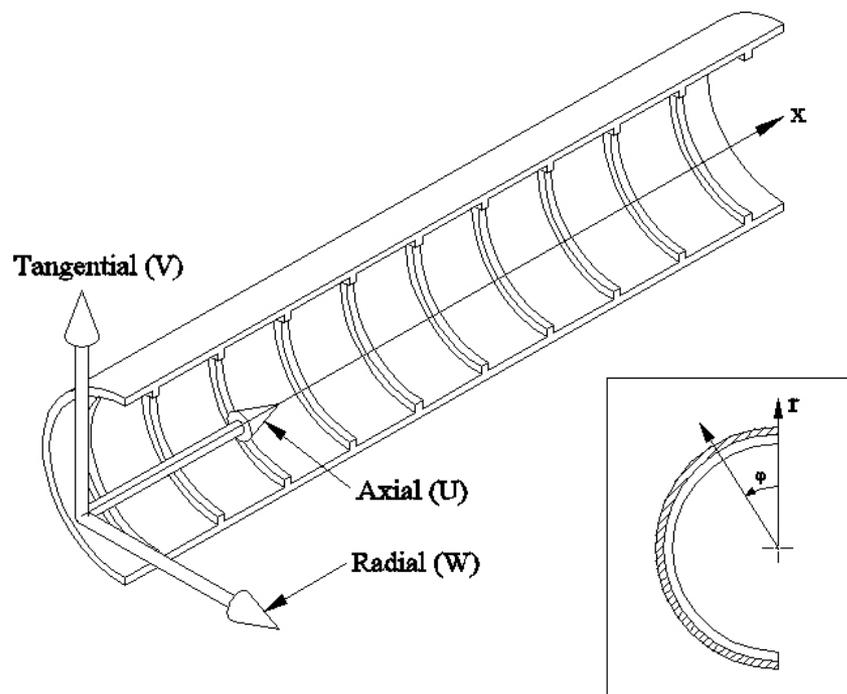
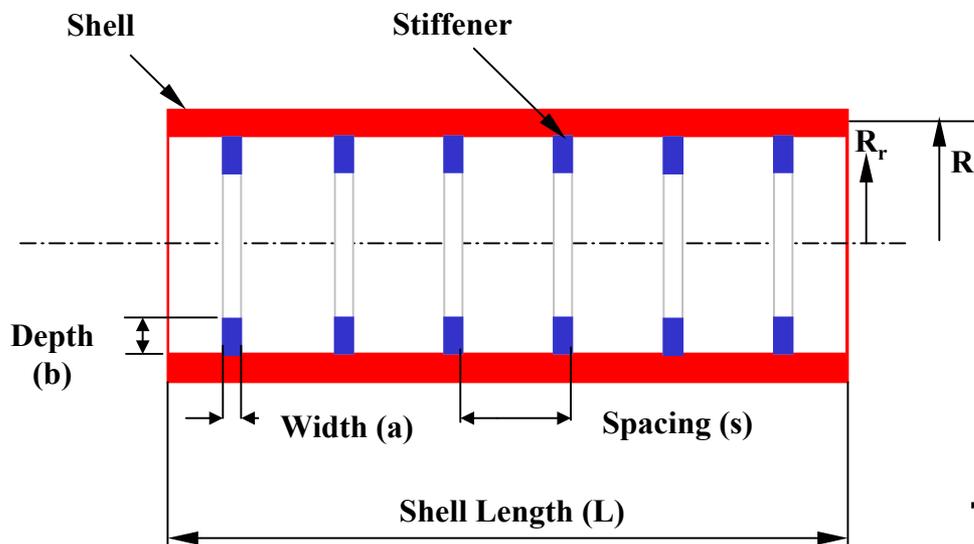
Multi-Disciplinary Design Optimization Strategies

Virtual Reality Environment

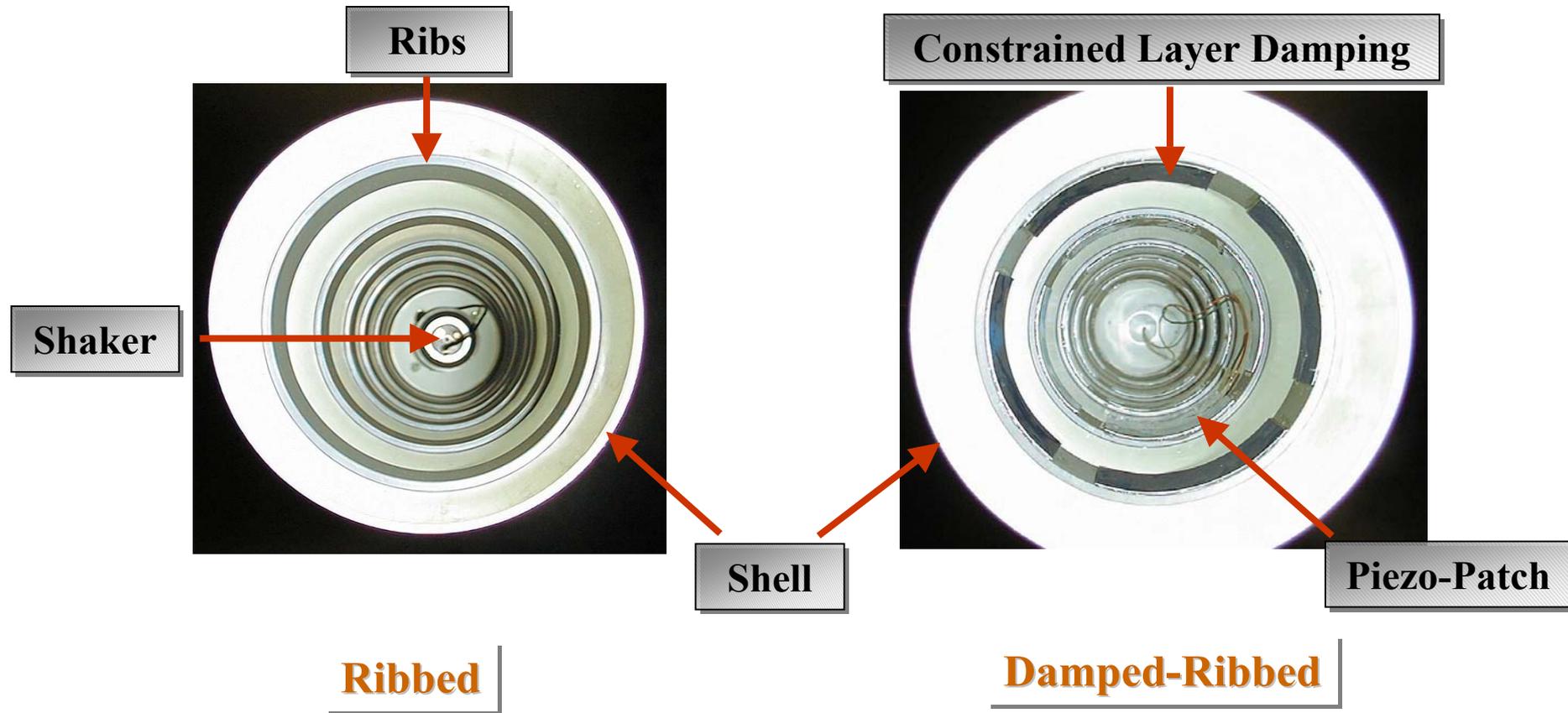
DESIGN OF UNDERWATER SHELLS



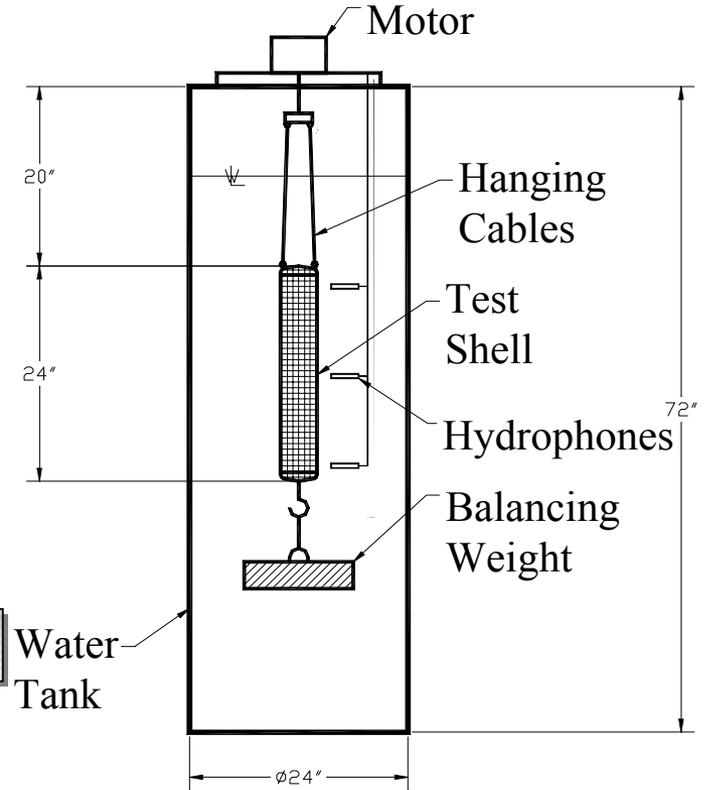
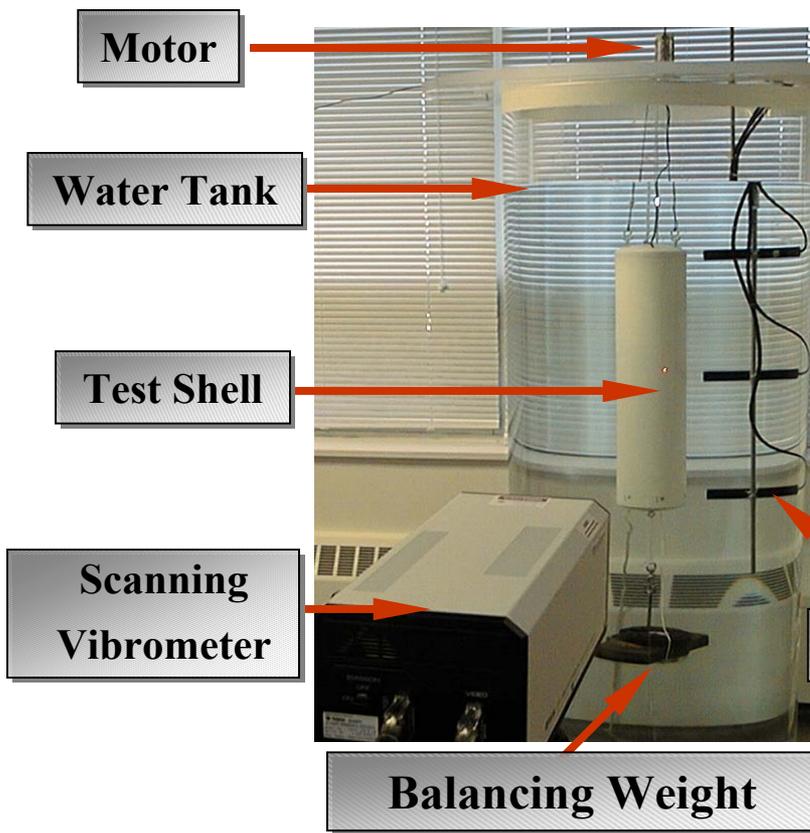
Stiffened shell configuration & geometrical parameters



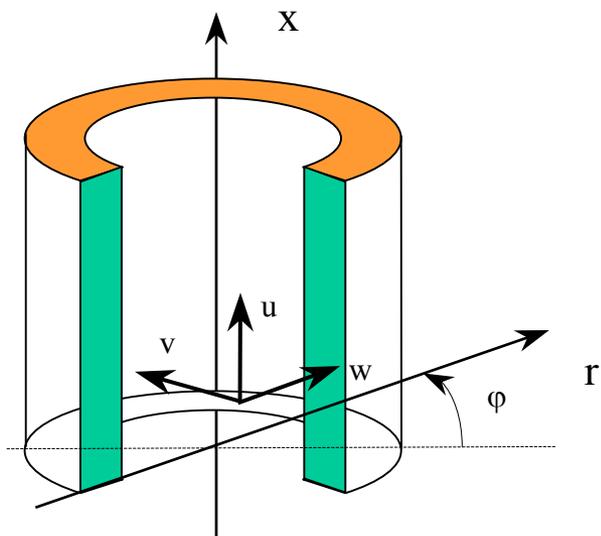
STIFFENED, DAMPED & ACTIVE SHELLS



TESTING OF STIFFENED, DAMPED & ACTIVE SHELLS

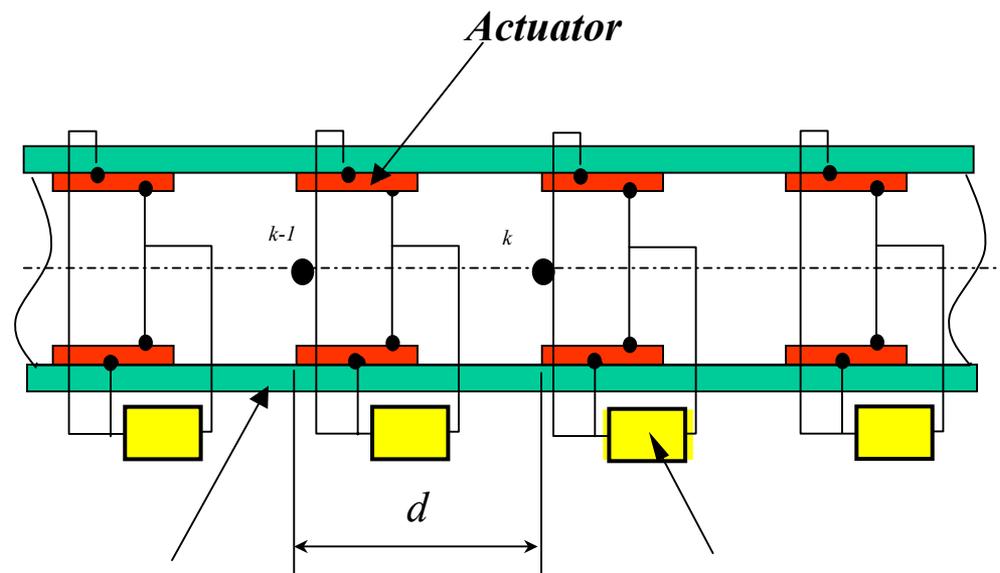


ACTIVE PERIODIC SHELL



Coordinate System

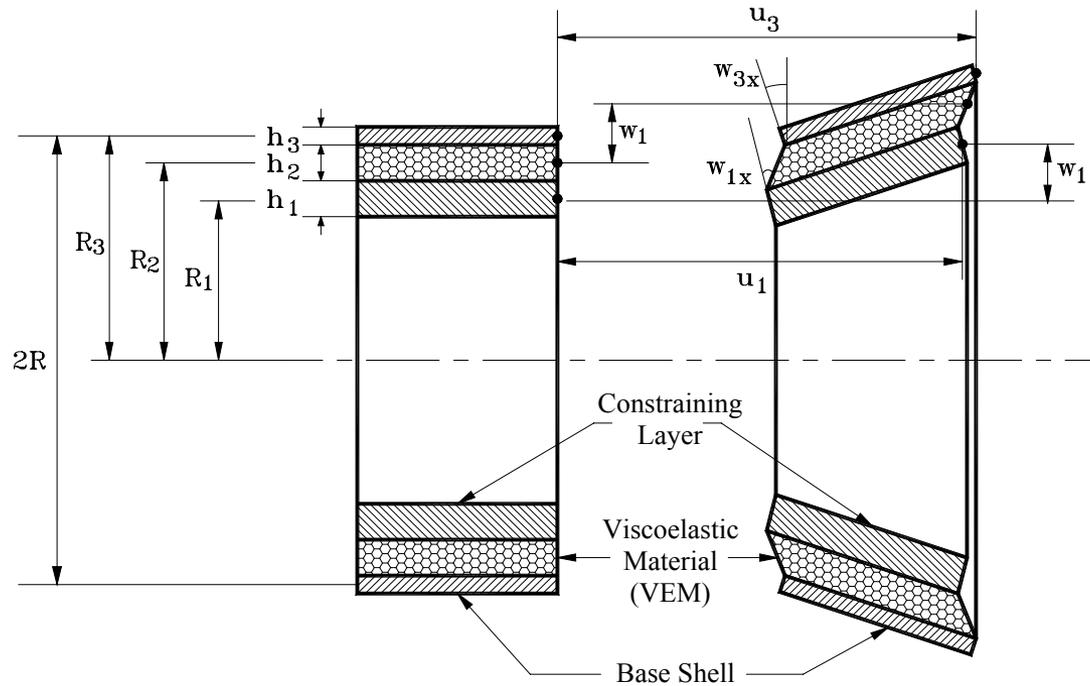
Active Periodic Shell Assembly



Base shell

controller

GEOMETRICAL AND KINEMATICAL PARAMETERS OF THE SHELL SYSTEM



FINITE ELEMENT MODELING

The nodal deflection vector is:

$$\{\delta(n, x)\} = \{u, v, w, w_x\}^T \cdot \cos(n\varphi)$$

where n = order of lobar mode, and φ = Circumferential angle

Equations of Harmonic Motion of Fluid-Loaded Shell:

$$\begin{array}{c}
 \text{Structural Stiff.} \quad \text{Control Stiff.} \quad \text{Structural Mass} \quad \text{Coupling Matrix} \quad \text{Structural Defl.} \quad \text{Loads} \\
 \downarrow \quad \downarrow \quad \downarrow \quad \downarrow \quad \downarrow \quad \downarrow \\
 \left[\begin{array}{cc}
 [K(n)] + [K_c(n)] - \omega^2 \cdot [M(n)] & -[\Omega(n)] \\
 -\rho_f \cdot \omega^2 \cdot [\Omega(n)] & [K_f(n)] - \omega^2 \cdot [M_f(n)]
 \end{array} \right] \cdot \begin{Bmatrix} \delta^{(e)}(n) \\ p^{(e)}(n) \end{Bmatrix} = \begin{Bmatrix} F(n) \\ 0 \end{Bmatrix} \\
 \uparrow \quad \uparrow \quad \uparrow \\
 \text{Fluid Stiff.} \quad \text{Fluid Mass} \quad \text{Fluid Pressure}
 \end{array}$$

Finite Element of Fluid-Loaded Stiffened Shells (cont.)

☑ For harmonic motion at frequency “ ω ”

$$([M(n)] + [M_a(n)]) \cdot \{\ddot{\delta}^{(e)}(n)\} + [K(n)] \cdot \{\delta^{(e)}(n)\} = \{F(n)\}$$

where $[M_a(n)] = \rho_f \cdot [\Omega(n)] \cdot [K_f(n)]^{-1} \cdot [\Omega(n)]^T$ **Added Mass**

☑ Pressure distribution

$$\{p^{(e)}(n)\} = \rho_f \cdot \omega^2 \cdot [K_f(n)]^{-1} \cdot [\Omega(n)]^T \cdot \{\delta^{(e)}(n)\}$$

Finite Element of Fluid-Loaded Stiffened Shells (cont.)

☑ External Loads (\mathbf{F})

$$\mathbf{F} = \underbrace{\mathbf{F}_e}_{\substack{\text{External} \\ \text{Loads}}} + \underbrace{\mathbf{F}_c}_{\substack{\text{Control} \\ \text{Forces}}}$$

where $\mathbf{F}_c = -\mathbf{K}_d \mathbf{S} \dot{\delta}$

$\mathbf{S} = \text{Actuator / Sensor Placement Matrix}$

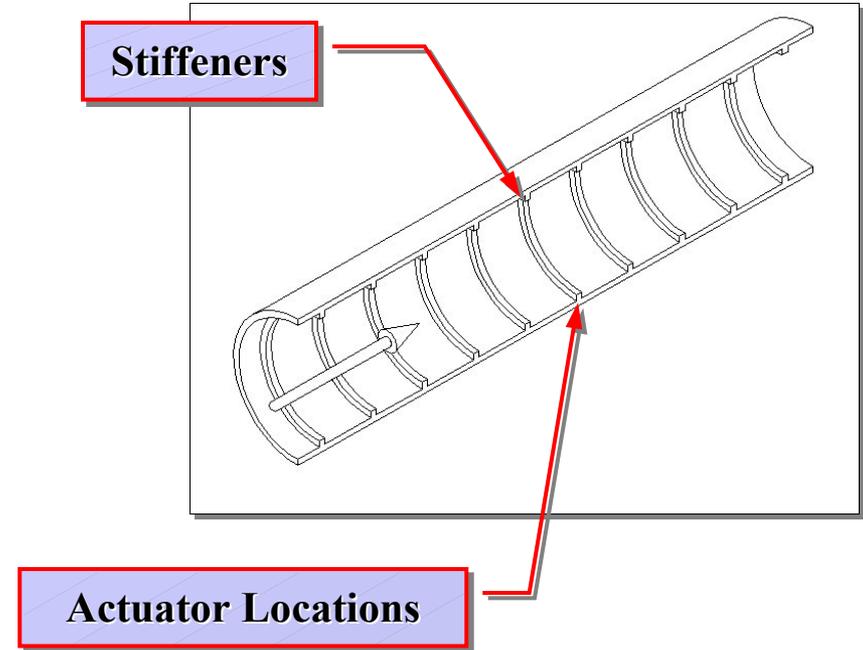
☑ Sound Intensity (\mathbf{I})

$$I(x, r, \varphi) = \frac{p^2(x, r, \varphi)}{2 \cdot \rho_f \cdot c}$$

Multi-Criterion Optimization (cont.)

Objective Functions (Minimize)

- Maximum Sound Intensity
- Maximum Radial Vibration Level
- Maximum Tangential Vibration Level
- Maximum Axial Vibration Level
- Cost of Passive Stiffeners
- Weight of Passive Stiffeners
- Cost of Added Actuators/Sensors
- Weight of Actuator/Sensor Mass
- Control Effort
- - Controllability
- - Observability



Multi-Criterion Optimization (cont.)

Constraints

No. of Stiffeners

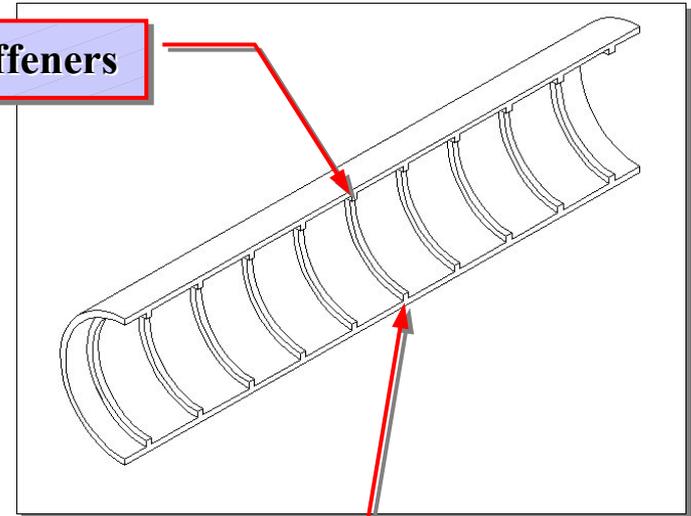
- No. of Actuators/sensors (N_a) $0 < N_a \leq N_s$
- Control Gain (K_d) $0 \leq K \leq 2 \times 10^5$

Design Variables

- Number of Actuators
- Actuator/Sensor Locations
- Control Gain

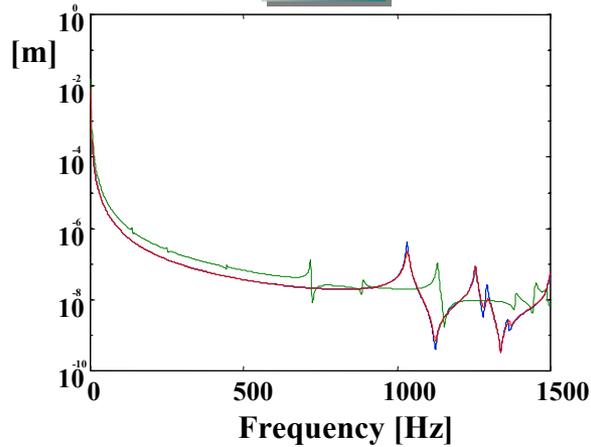
Stiffeners

Actuator Locations



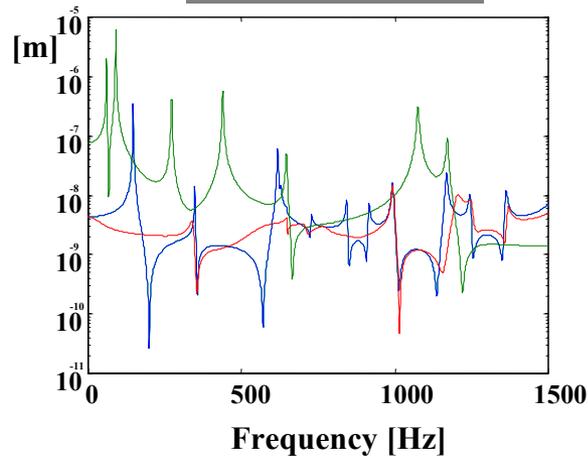
Configuration 3: 3 Actuators on Ribs 1-3-7, $K_d=3,100$ (All design Objectives)

Axial

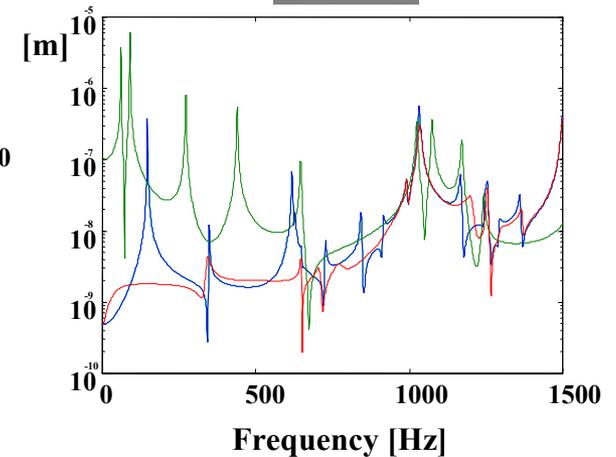


Vibration FRF

Circumferential



Radial

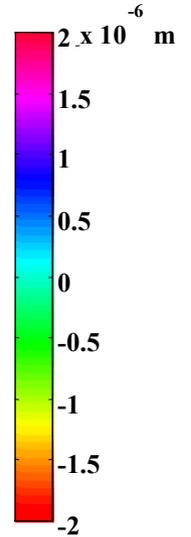
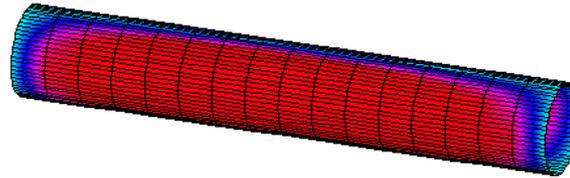


- Plain Shell
- 7 stiffeners - Uncontrolled
- 7 stiffeners - Controlled

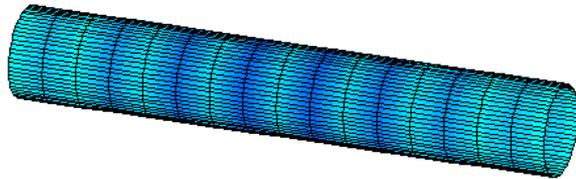
Configuration 3: 3 Actuators on Ribs 1-3-7, $K_d=3,100$ (All design Objectives)

Shell Vibration

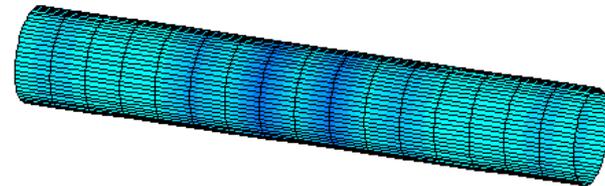
Plain



7 Stiffeners - Uncontrolled

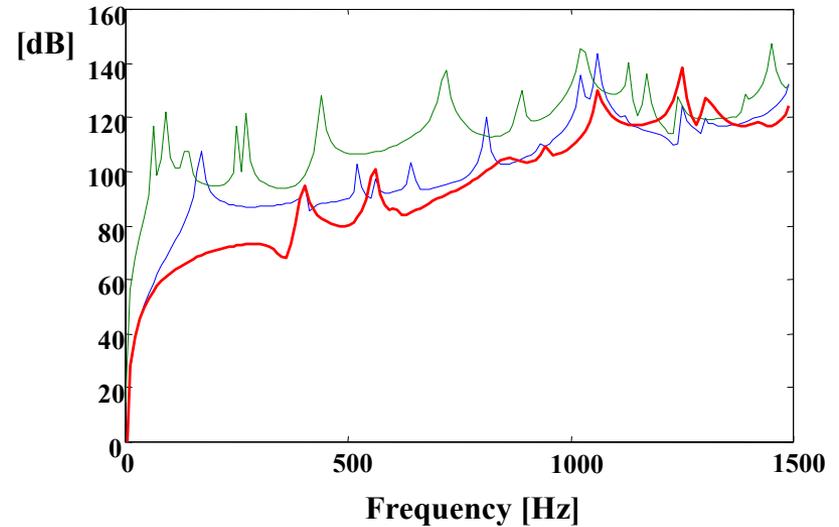


7 Stiffeners - Controlled



Configuration 3: 3 Actuators on Ribs 1-3-7, $K_d=3,100$ (All design Objectives)

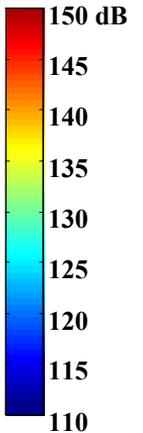
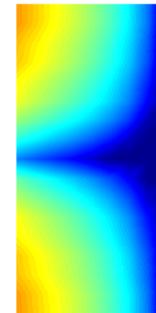
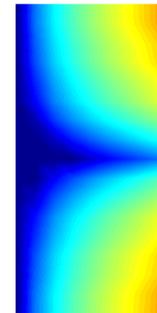
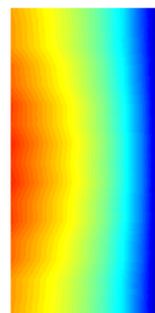
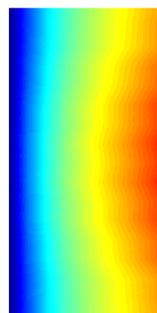
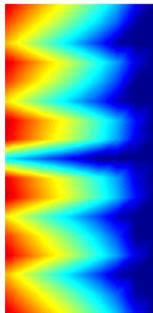
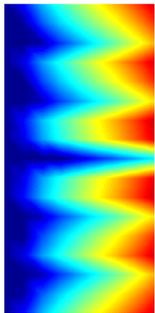
Sound Intensity



Plain

7 Stiffeners - Uncontrolled

7 Stiffeners - Controlled



VIRTUAL REALITY DESIGN OF A TORPEDO SHELL



WHY VIRTUAL REALITY ENVIRONMENT ?

- Today's interfaces (keyboard, mouse, monitor, etc.) force us to working within tight, unnatural, two-dimensional constraints.
- In **Virtual Reality (VR)**, *human-computer interface technology* leverages the *natural human capabilities*.
- **VR** provides engineers with real-time 3D audio, visual & sensory perception in a more intuitive & natural manner.
- In VR, engineers can look and move around/inside a virtual model or environment, drive through it, lift items, hear things & feel things.



MISSION OF VIRTUAL REALITY LABORATORY



Interactive & Collaborative Design of SMART Structures in:

■ **Real time**

■ **Environment with:**

virtual reality audio,

visual, and

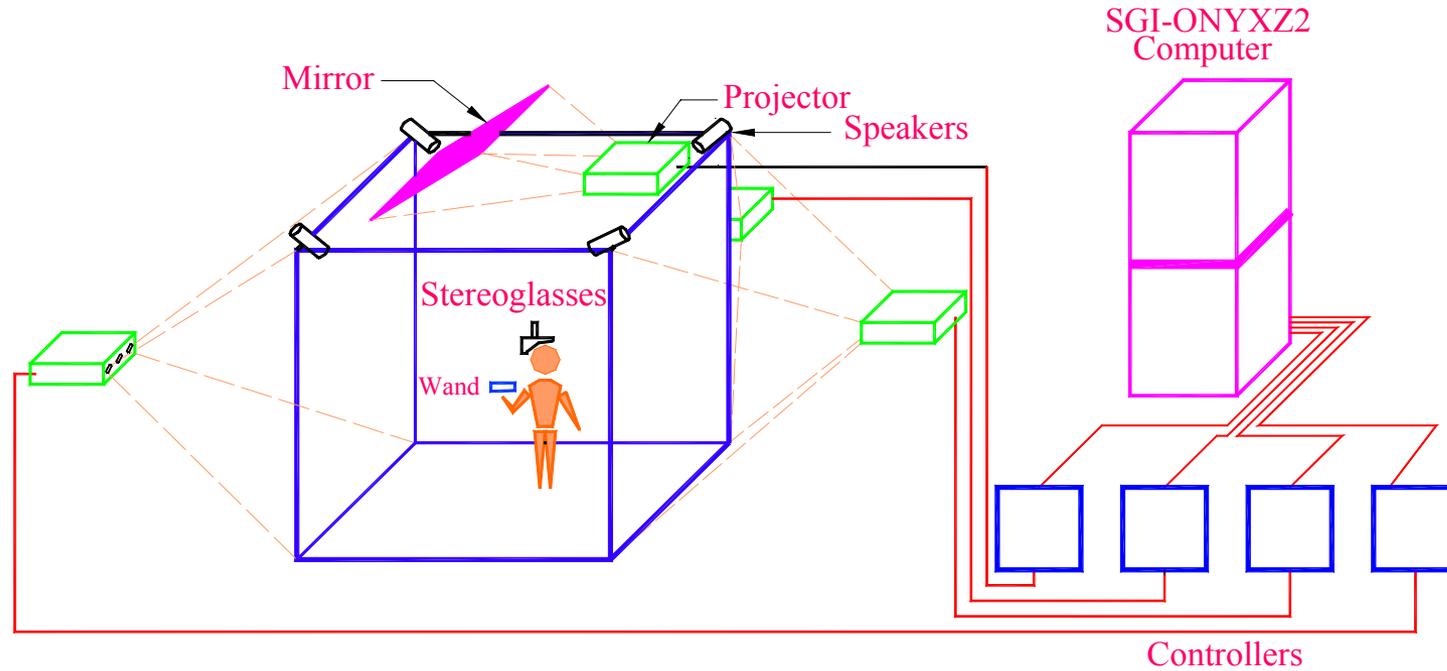
sensory capabilities.

DESIGN IN VIRTUAL REALITY ENVIRONMENT

- **Design is Interactive with Designer in the Loop**
- **Vary design parameters & monitor response in real-time**
- **Collaborative Design with other design sites**

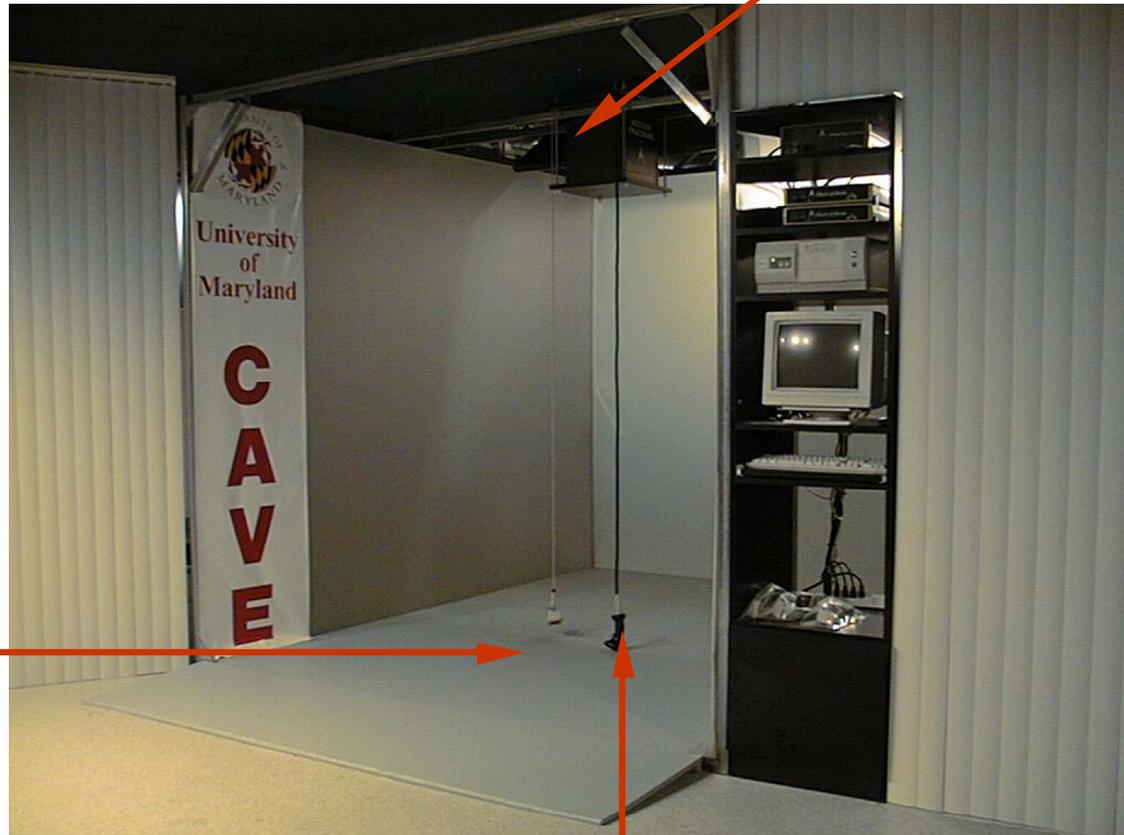


COMPUTER-AUTOMATED VIRTUAL ENVIRONMENT



UMCP VIRTUAL REALITY LAB

Tracking System



Goggles

Wand

University of Maryland



COMPUTER SYSTEM OF VIRTUAL REALITY LAB



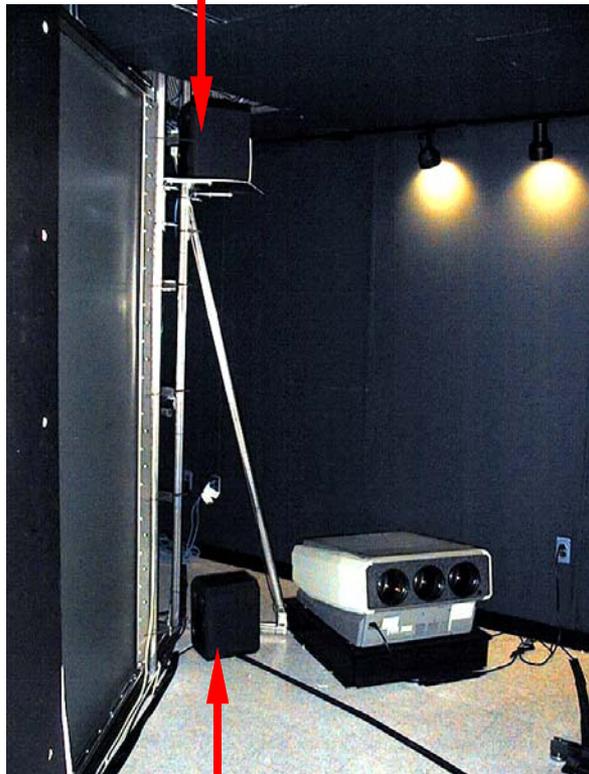
**SGI/ONYX2
COMPUTER**

VIRTUAL REALITY LAB – USERS ROOM

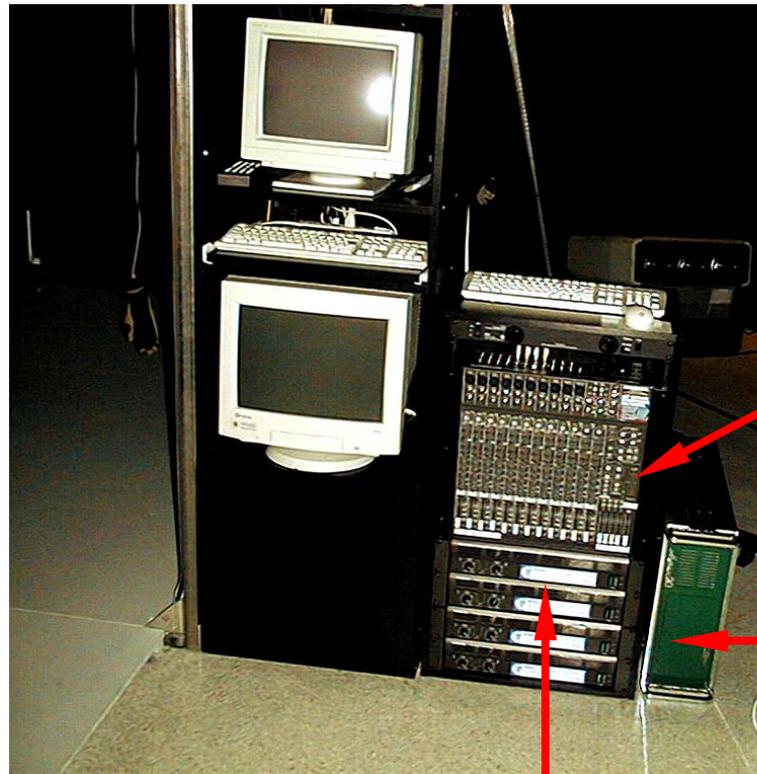


VIRTUAL REALITY LAB - ACOUSTICS

Top Speakers



Bottom Speakers

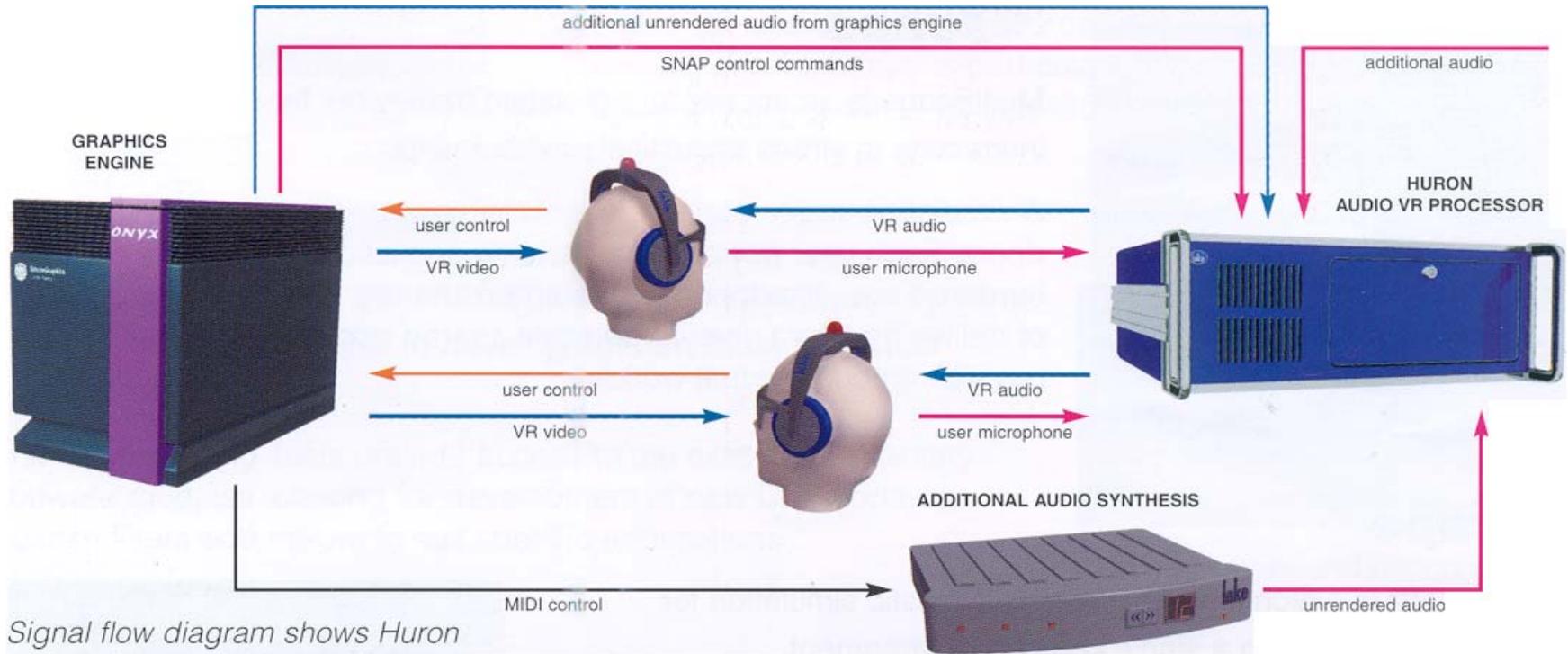


Mixers

Virtual Acoustics System

Power Amplifiers

COMPUTER-AUTOMATED VIRTUAL ENVIRONMENT



Signal flow diagram shows Huron system integrated into a VR simulation environment.



CYBER TOUCH GLOVES

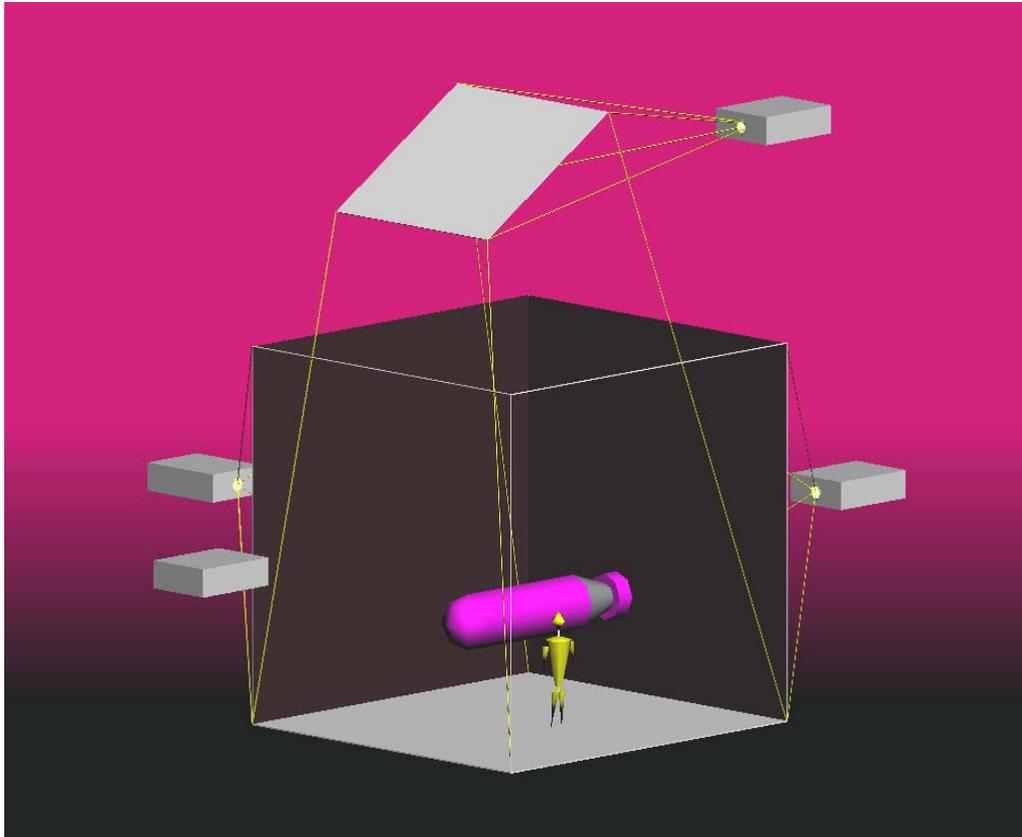


The Glove has six small vibro-tactile stimulators on the fingers and the palm.

Each stimulator can be individually programmed to vary the strength of touch sensation.

VIRTUAL DESIGN OF ACTIVE STRUCTURES

Torpedo

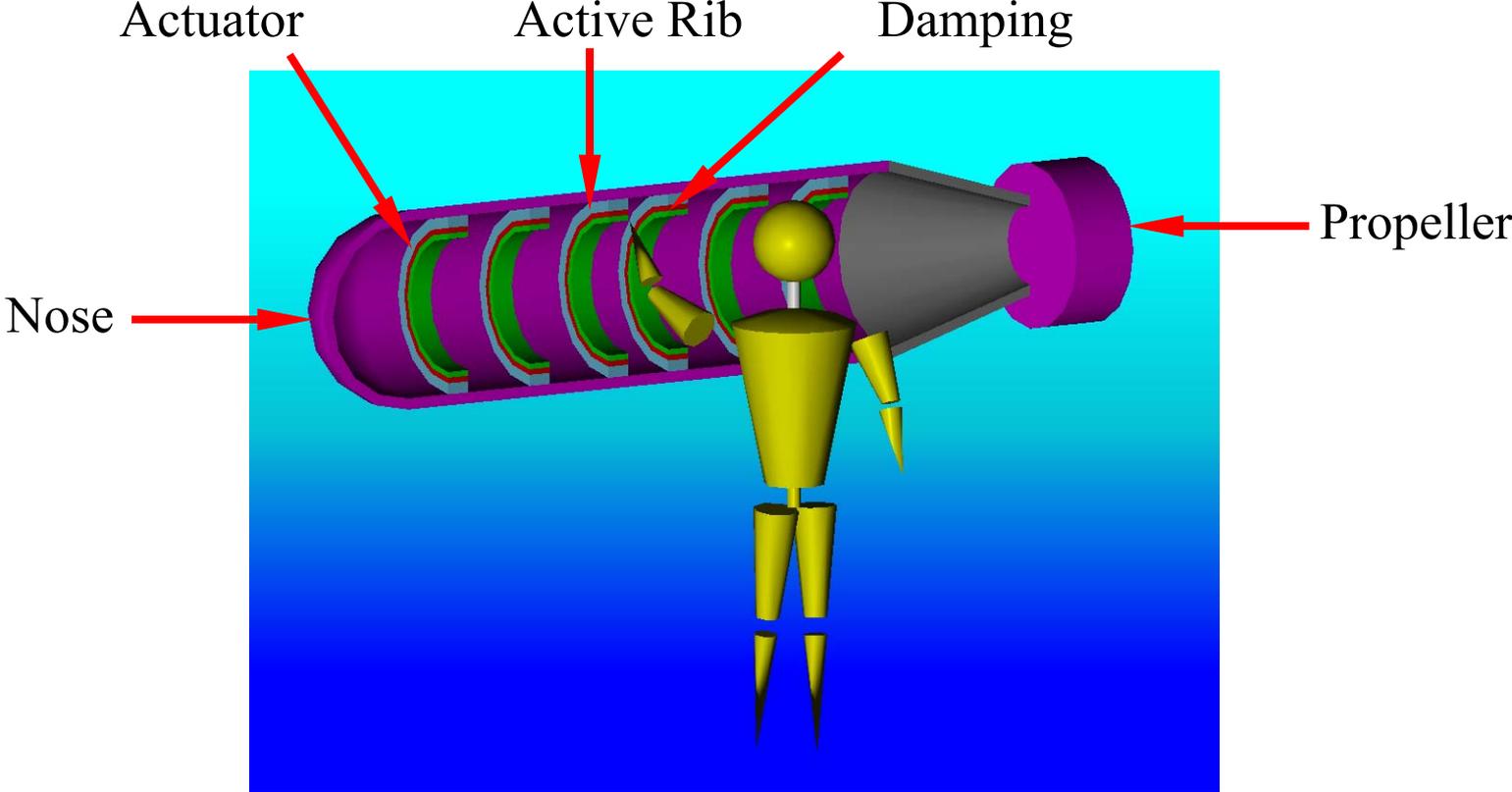


VIRTUAL DESIGN OF A TORPEDOE SHELL

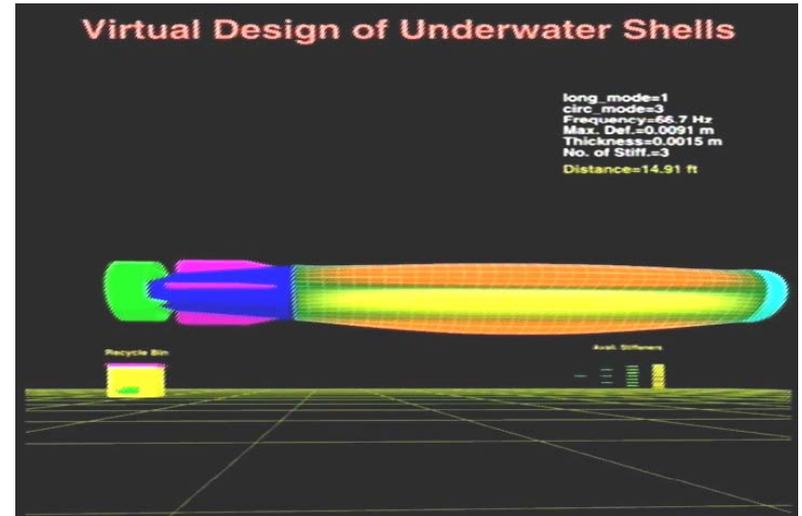
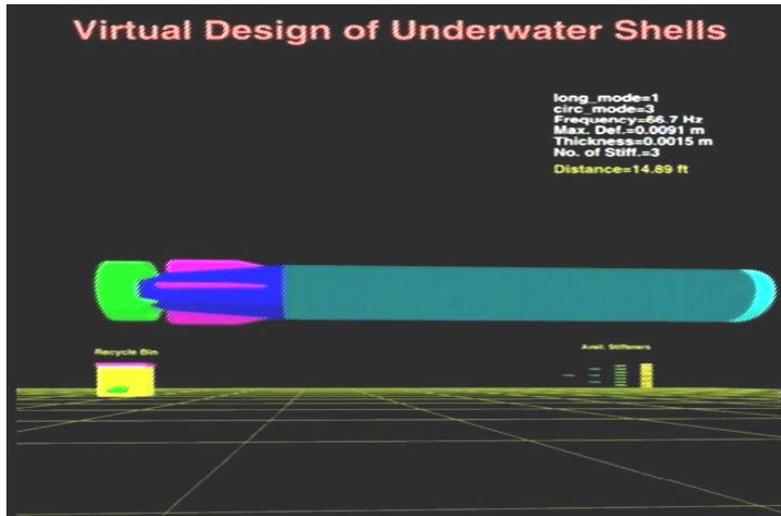


Implementation of virtual reality on SGI/ONYX2 Computer

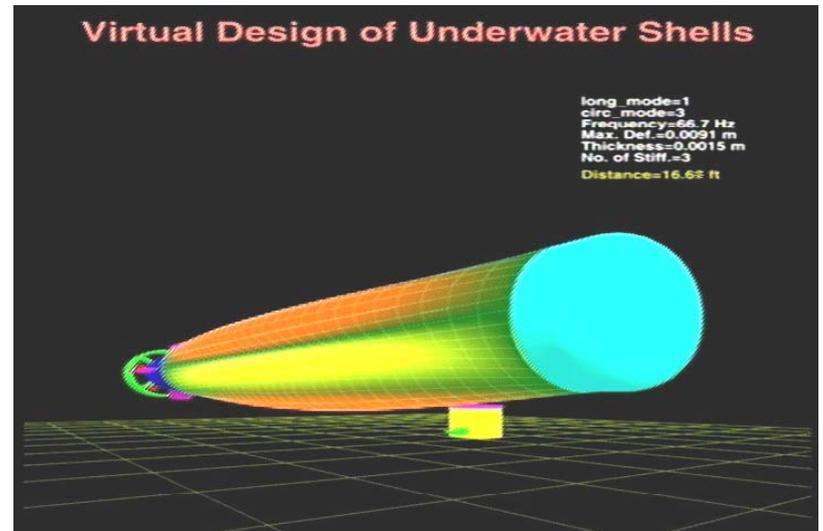
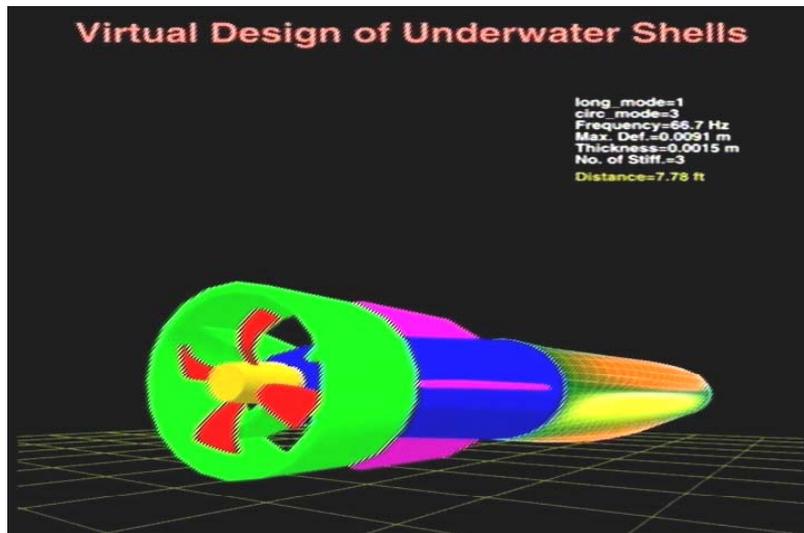
VIRTUAL DESIGN OF ACTIVE TORPEDOES



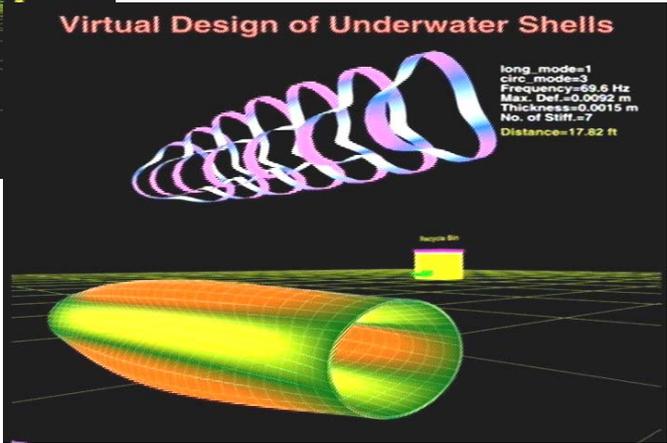
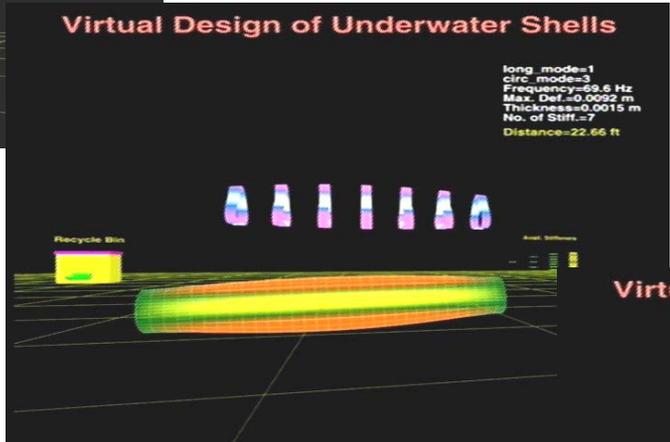
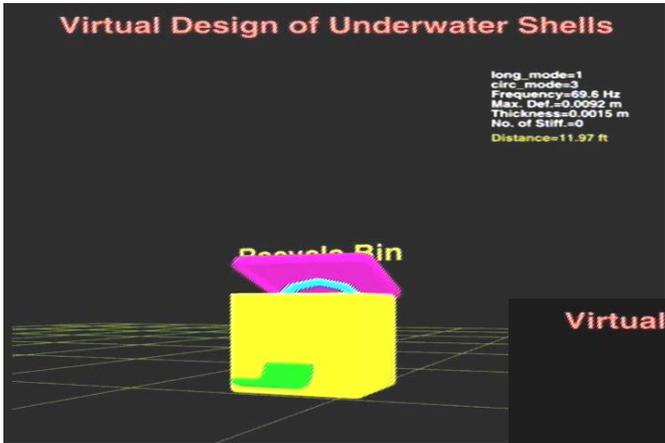
VIRTUAL DESIGN OF A TORPEDO SHELL



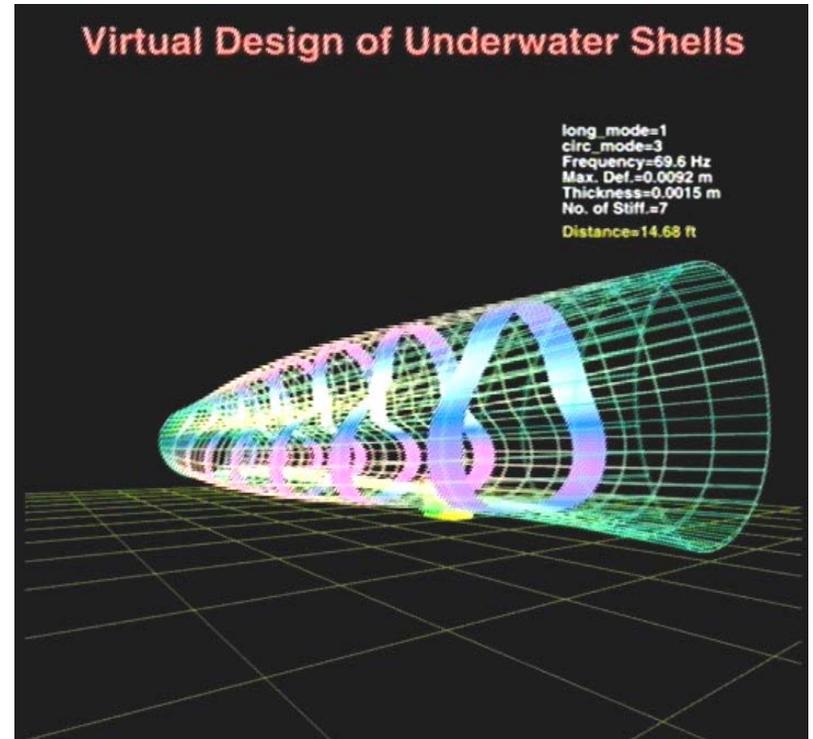
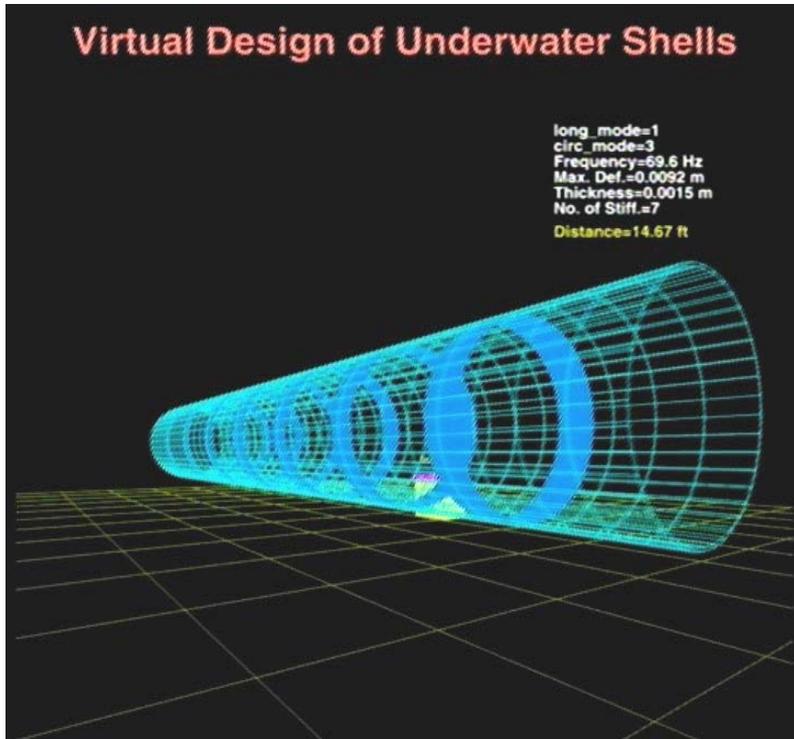
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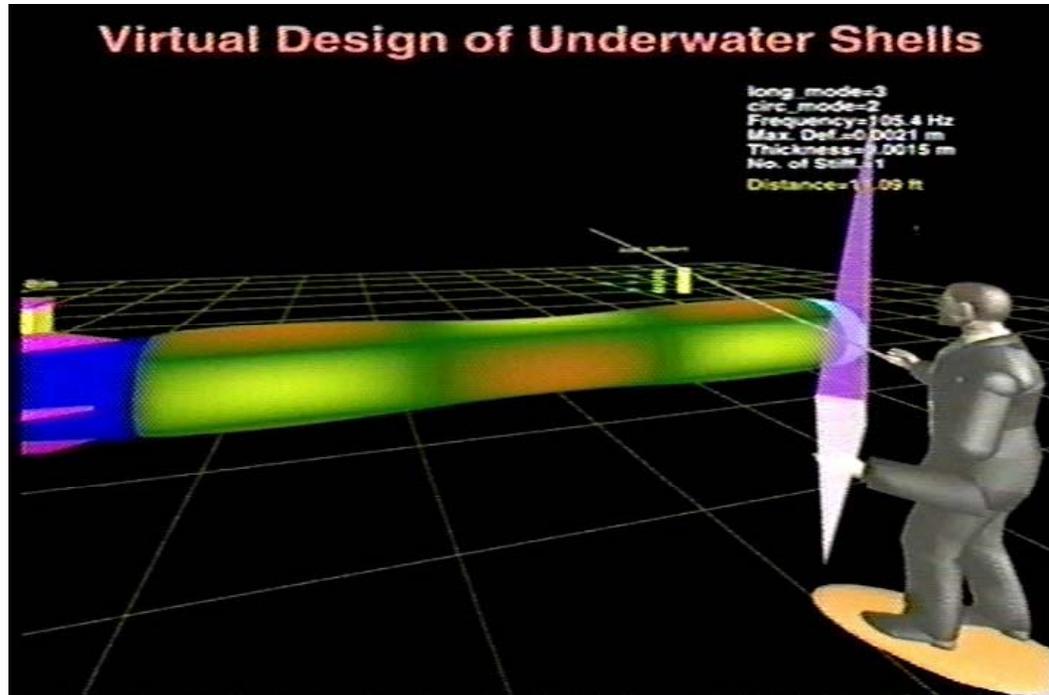
VIRTUAL DESIGN OF A TORPEDO SHELL



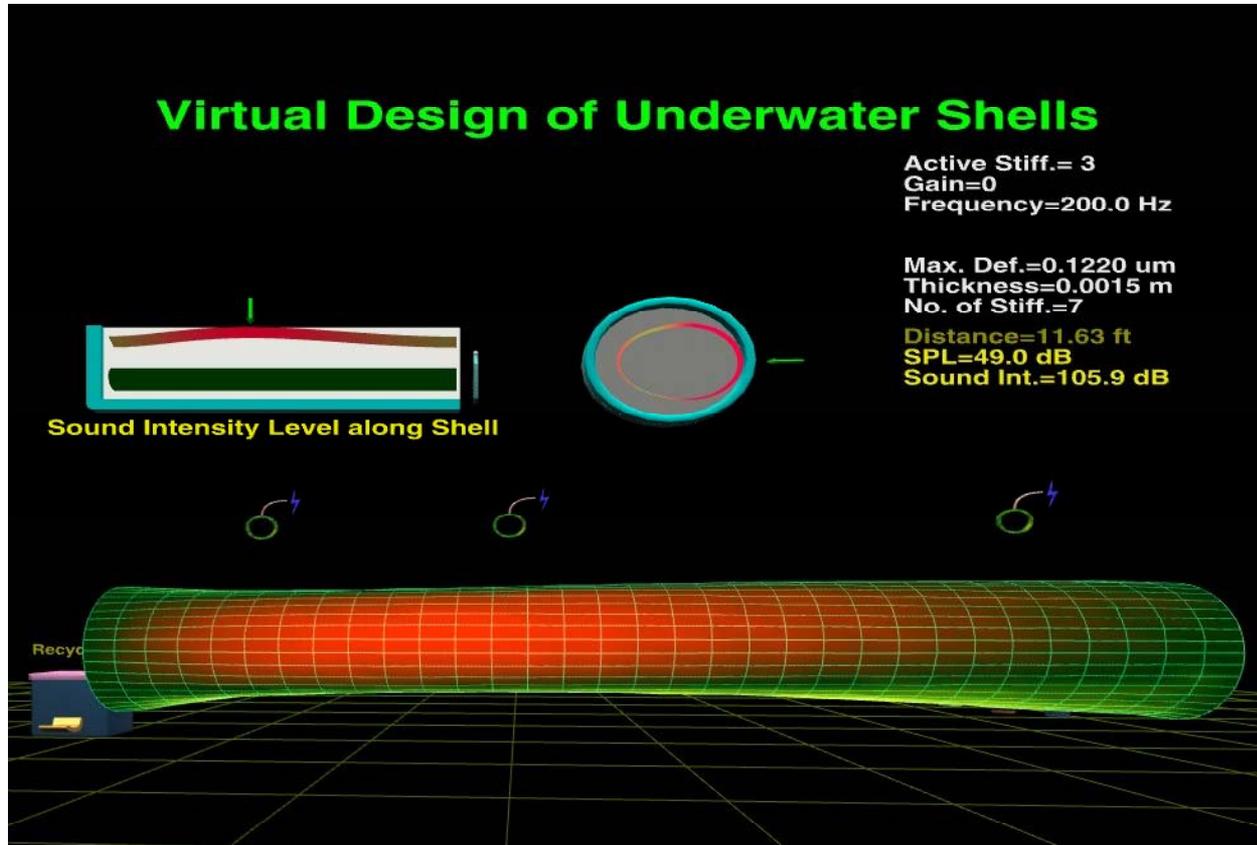
VIRTUAL DESIGN OF A TORPEDO SHELL



COLLABORATIVE DESIGN OF A TORPEDO SHELL

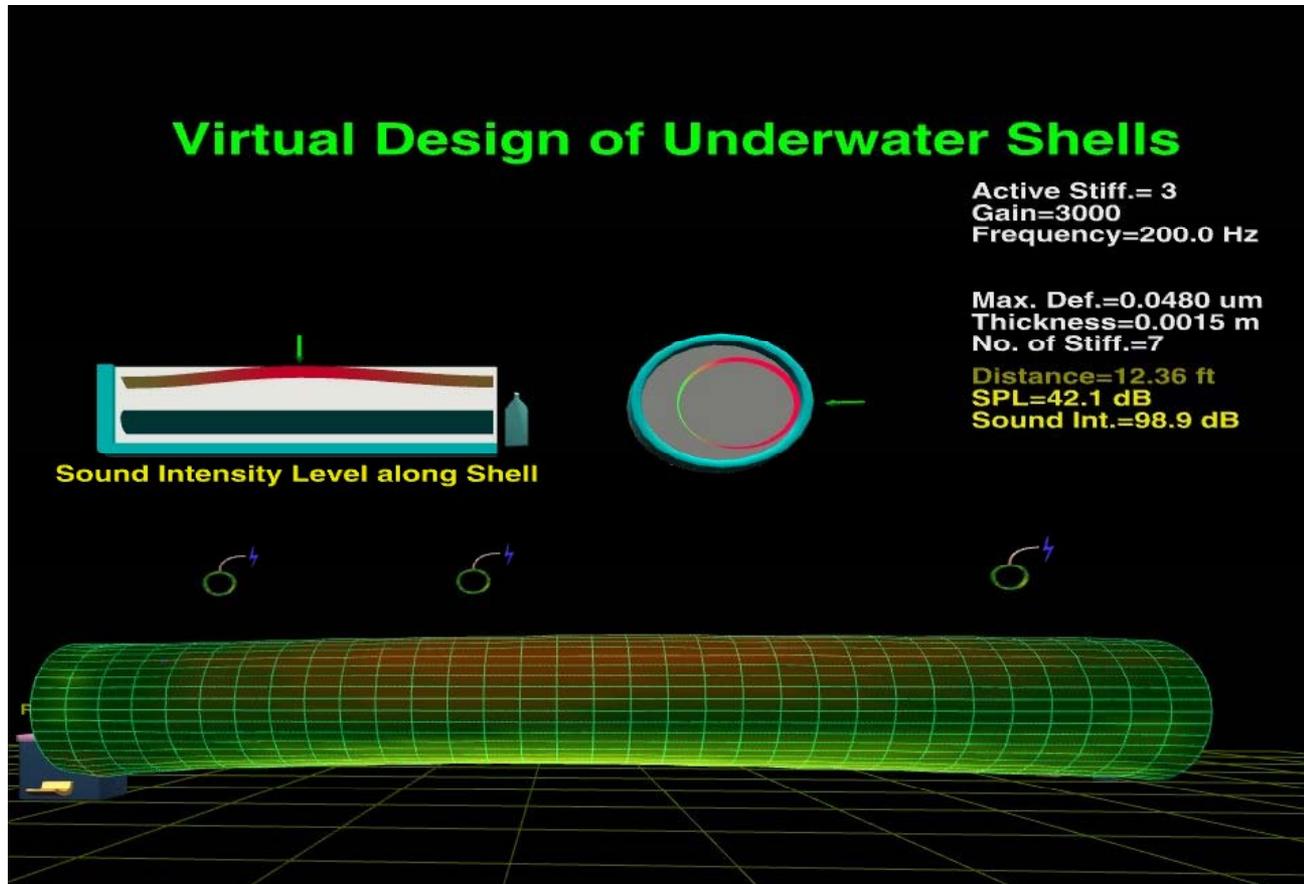


No. of stiffeners = 7, Active Stiffeners: 1,3, 7, Frequency 200 Hz



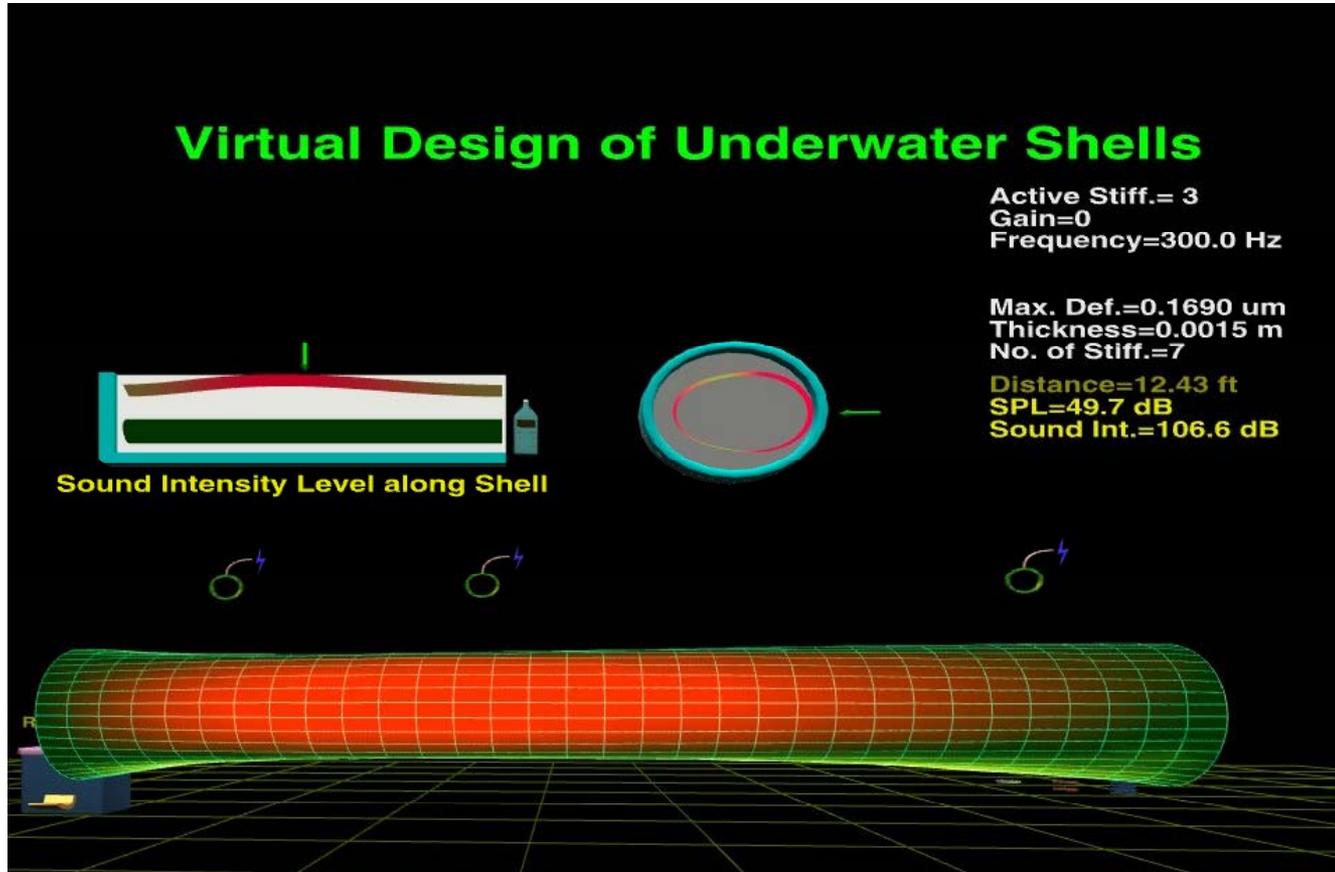
Gain = 0

No. of stiffeners = 7, Active Stiffeners: 1,3, 7, Frequency 200 Hz



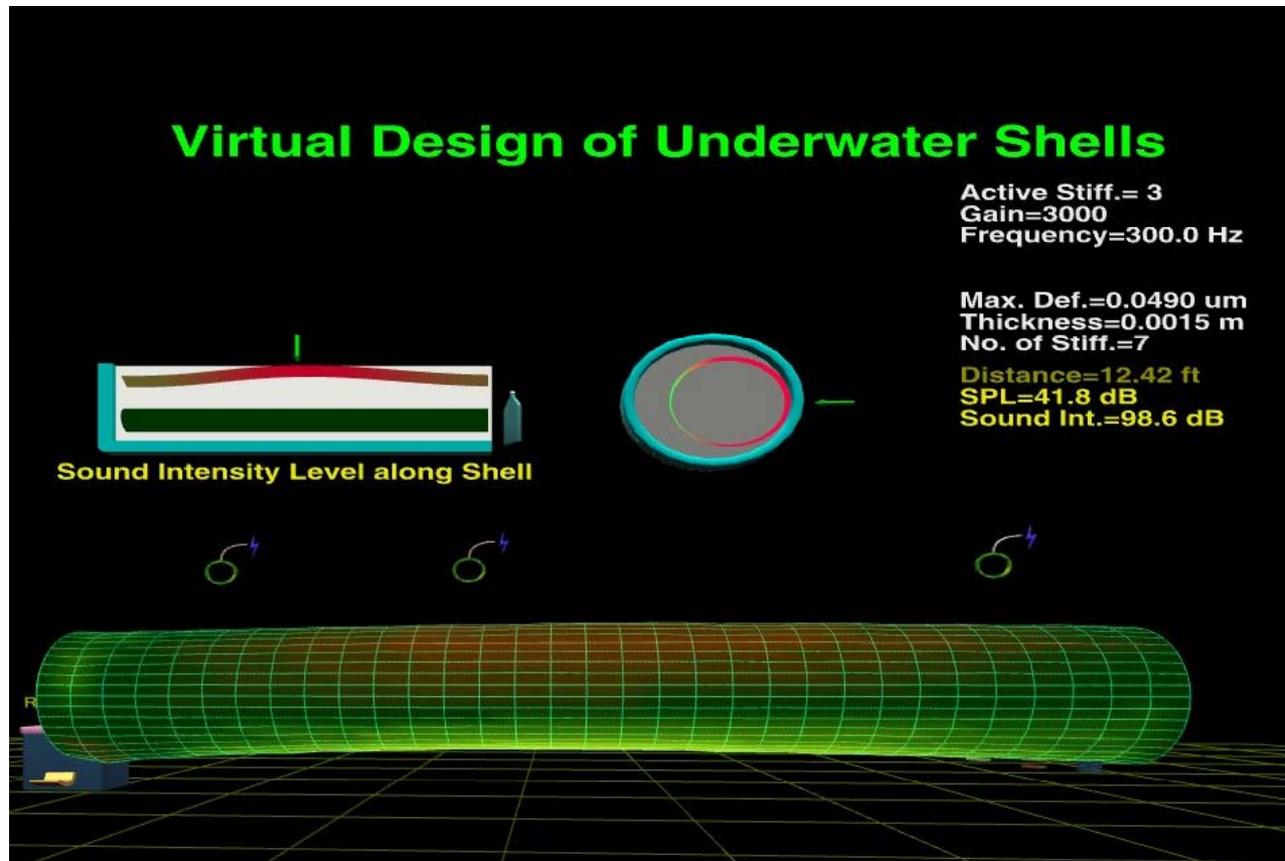
Gain =3000

No. of stiffeners = 7, Active Stiffeners: 1,3, 7, Frequency 300 Hz



Gain = 0

No. of stiffeners = 7, Active Stiffeners: 1,3, 7, Frequency 300 Hz



Gain =3000

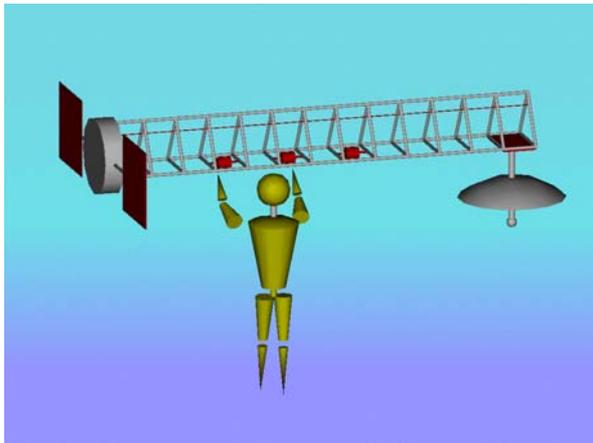
VIRTUAL DESIGN OF A TORPEDO SHELL



FUTURE APPLICATIONS



Car Crash

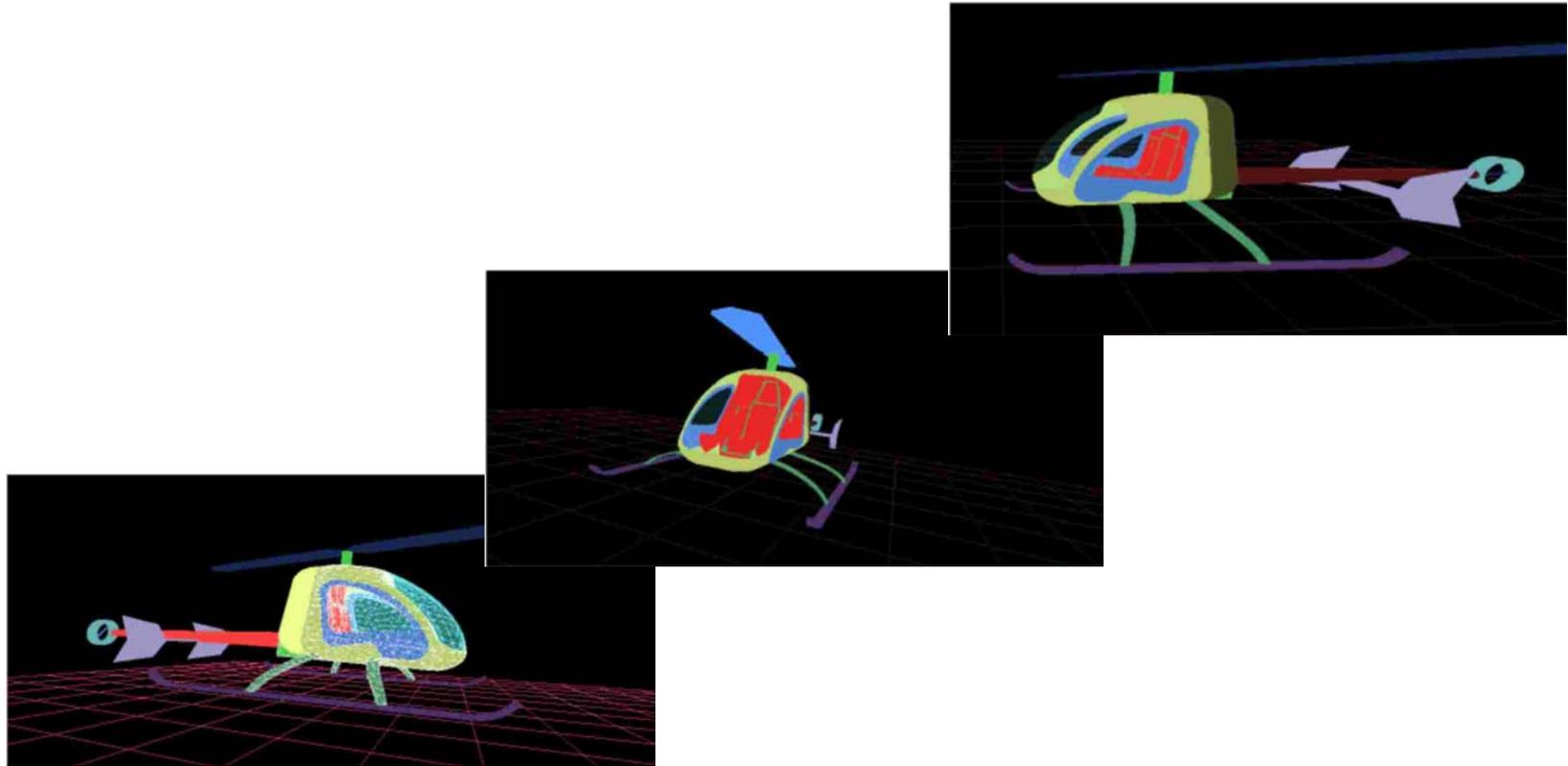


Space Structures

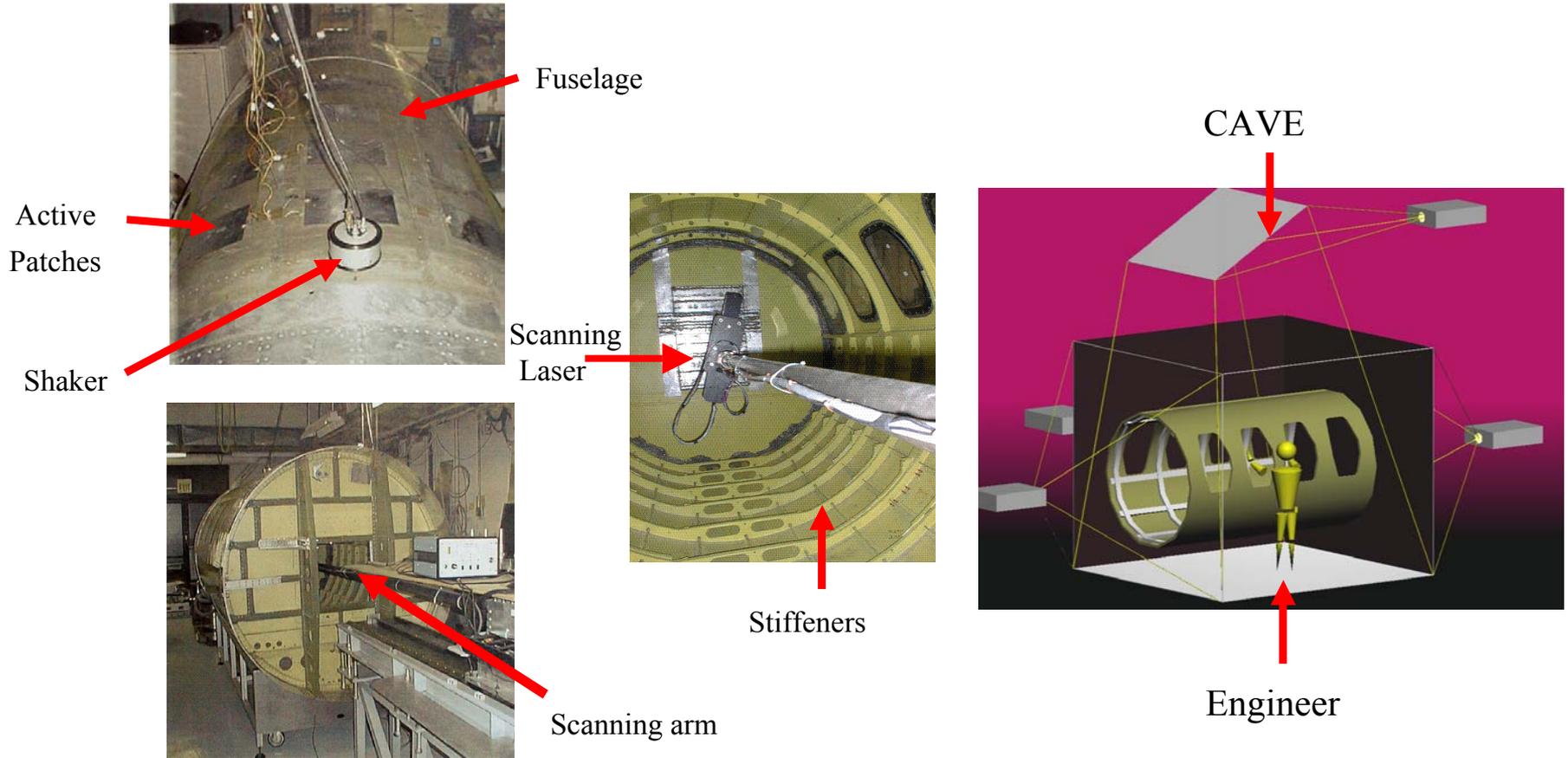


Vehicle Dynamics & Acoustics

Virtual Reality Design of Helicopter Noise & Vibration Controls



Cessna Citation II Fuselage



Conclusions

1. Underwater Shells with Active stiffeners are designed using Multi-Disciplinary Optimization (MDO).
2. The optimal design parameters of the Actuator/sensor pairs (**Number, Location & Control Gain**) are determined in order to minimize the sound radiation, the structural vibration, weight, production & life cycle cost, control effort & maximize controllability & observability.



END